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Republic Aviation Corp., Farmingdale, L. I., N. Y. (Report No. EDR-C
905-104)

Analog Computer Investigation of Stability of F-84 - B-29 Wing Tip
Coupling

Helfman, S. 11 May '51 137pp tables, diagrs, graphs

Airplanes - Stability

Aerodynamics (2)

Airplanes - Control

Stability and Control (1)

Airplanes - Wing-tip

coupling

Project MX-1016

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REPUBLIC AVIATION CORPORATION
FARMINGDALE, LONG ISLAND
NEW YORK

ANALOG COMPUTER INVESTIGATION

OF

STABILITY OF F-84 + B-29 WING TIP COUPLES

PROJECT MX-1016

R&D REPORT R&D-0905-104

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Analog Computer Investigation of

Stability of F-84 - B-29 Wing Tip Coupling

Project MI-1016

RAC Report No. EDR-C905-104

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May 11, 1951

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I. Introduction

The incorporation of the adjustable rear latch and the single aileron method of control into the design of the wing tip coupling mechanism has necessitated the extension of the analysis of the stability of the combination to include the effect of altitude, speed, weight ratios, and control ratios.

This report presents the results of an analog-computer investigation of the level-flight stability of the F-84 - B-29 coupling scheme undertaken at the Office of Air Research, Wright-Patterson Air Forces Base, Dayton, Ohio, during the week of November 27, 1950.

Subsequent analysis of the two-point method of control using an increased number of degrees of freedom has indicated unstable motion; hence the results given in this report should be reviewed with this fact in mind. An alternative method of control, using auto-pilot components and a single-point method of attachment, is now in the process of investigation and will eventually supersede the two-point method of control analyzed in this report.

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II. Summary

The motions resulting from symmetrical disturbances and also from anti-symmetrical disturbances were obtained for 270 possible flight conditions in accordance with the schedule of runs given in Table I. The results of the analysis are tabulated in Table III, for the four-degree of freedom systems investigated. In all of the 540 conditions analyzed, the resultant motions of the flexible combinations with single aileron control were stable and amply-damped, confirming the advisability, at least theoretically, of using single aileron control. Figure II(a) and II(b) are representative of the records obtained from the computer.

Subsequently, the addition of a fifth degree of freedom to the equations of motion for a symmetric disturbance, namely, ability of the B-29 airplane to translate vertically, has resulted in unstable motion (See Fig. III(a) and (b)), and has necessitated an analytical study of the one-point method of attachment previously mentioned.

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Absent - 136**

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Present - 137**

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I. Coefficients & Symbols

M	Mass of B-29 Airplane, slugs
m	Mass of F-84 Airplane, slugs
q	Dynamic Pressure = $\frac{1}{2} \rho v^2$, lbs. per sq. ft.
v	Velocity, ft. per sec.
I_{x-x}	Roll Moment of Inertia of B-29 Airplane, slugs-ft. ²
I_{y-y}	Pitch Moment of Inertia of B-29 Airplane, slugs-ft. ²
k_x	Radius of Gyration of F-84 Airplane in Roll, ft.
k_y	Radius of Gyration of F-84 airplane in Pitch, ft.
a	Distance from elastic axis of B-29 wing tip to F-84 center of gravity (Fig. I), ft.
c	Distance from B-29 center of gravity to B-29 wing elastic axis measured at wing tip, ft. = 3.25 ft. for .26 MAC B-29 center of gravity.
l_{t₂₉}	Distance from B-29 center of gravity to center of pressure of horizontal tail, ft.
l_{t₈₄}	Distance from F-84 center of gravity to center of pressure of horizontal tail, ft.
R	Semi-span of B-29 airplane, ft.
r	Semi-span of F-84 airplane, ft.
C.G.	Center of gravity position of F-84 airplane, fraction of MAC.
x	Maximum value of pitch disturbance over B-29 airplane, ft/sec.
y	Maximum value of pitch disturbance over F-84 airplane, ft/sec.
z	Maximum value of rolling disturbance, ft./sec.
K	Automatic Aileron drive ratio = $\frac{\text{aileron deflection}}{\text{flapping deflection}}$
X	$e^{-4.75t} [1 - e^{-5t}]$

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- w Vertical displacement of B-29 center of gravity, ft.
φ Roll displacement of B-29 wing, radians
θ Pitch displacement of B-29 airplane, radians
γ Bending displacement of B-29 wing tip relative to fuselage, ft.
δ Slope of B-29 wing tip in bending, radians
β Flapping deflection of P-84 airplane, radians
α Torsional deflection of B-29 wing tip relative to
fuselage, radians
 $\dot{\theta}$, $\ddot{\theta}$, etc. $\frac{d\theta}{dt}$, $\frac{d^2\theta}{dt^2}$, etc.

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VI. DiscussionA. Equations of Motion

The general form of the equations of motion given in Tables II-A and II-B is used to compute the system of differential equations (Tables II-D) that are solved on the analog computer. The possible degrees of freedom are shown in Figure I, from which the equations of motion are derived through an application of Newton's Law; namely:

$$\sum m_i a_i = \sum \text{External Forces} - - - - - \quad (1)$$

$$\sum m_i a_i x_i = \sum \text{External Moments} - - - - - \quad (2)$$

where:

 m_i is the mass of a particle a_i is the absolute acceleration of the particle considered x_i is an arm of the particle from an axis under consideration.

Replacing the acceleration, a_i , by its equivalent in terms of the mode variables, and neglecting products of the variables and their derivatives (small perturbations), leads to the set of equations of Table II-A and II-B.

Symmetric motion is caused by a symmetrical vertical gust disturbance and implies that no roll (ϕ) occurs. Similarly, anti-symmetric motion implies no pitch of the B-29 airplane (θ), and no vertical translation of the B-29 center of gravity (w).

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The results shown in Table III-A for symmetric motion were obtained for a four degree of freedom system containing θ , y , β , and α variables [since $\delta = f(y)$], assuming that the influence of W upon the resultant motion was negligible. Subsequent analysis indicated otherwise.

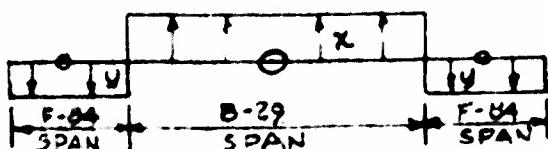
The results shown in Table III-B for anti-symmetric motion were obtained for a four degree of freedom system consisting of θ , y , β , and α variables.

B. Gust Disturbances

The design gust distributions considered in this report consist of vertical gusts having symmetrical and anti-symmetrical components. The motion resulting from a horizontal gust has not been treated here, but is amenable to analytic solution and had been previously computed. Since the equations of motion are linear, the total motion in any variable is the vectorial sum of that caused by the symmetrical gust (Table III-A) and that caused by the anti-symmetrical gust (Table III-B).

The symmetrical gust distribution is:

Spanwise:

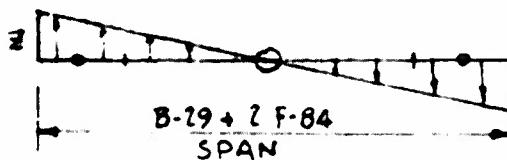


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where the maximum values of x and y are obtained from the table below:

Altitude	$X_{max.}$	$Y_{max.}$
Sea Level	14.0 ft/sec	7.3 ft/sec
20,000 ft.	17.1 ft/sec	8.9 ft/sec
35,000 ft.	21.0 ft/sec	10.8 ft/sec

The anti-symmetrical gust distribution is:



where the maximum value of Z is obtained from the table below:

Altitude	$Z_{max.}$
Sea Level	6.8 ft/sec
20,000 ft.	9.2 ft/sec
35,000 ft.	12.0 ft/sec

The variation of the gust magnitude, both symmetrical and anti-symmetrical, with time is given by:

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} x_{max.} \\ y_{max.} \\ z_{max.} \end{bmatrix} \cdot -4.75t \left[1 - e^{-5t} \right]$$

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where $e^{-4.75t} [1 - e^{-0.5t}] = I$, and corresponds to a gust gradient distance of approximately ten B-29 mean aerodynamic chord lengths.

2. Results of Analog Computer Investigation

The maximum values of the resultant oscillations are given in Table III-A for symmetrical motion, and in Table III-B for the anti-symmetrical motion. These values were obtained from the computer records of the 540 runs, a typical one being shown in Figure II-A and Figure II-B for Runs #121, 122, and 123.

The results indicate that single-aileron operation would provide satisfactory and stable motion, and that the effect of increasing K , which is the ratio of aileron deflection , is to reduce the maximum magnitude of the flapping deflection, β .

The resultant motion produces tip loads and moments on the B-29 wing tip which are given by:

$$\Delta \text{ Vertical Reaction Load at Neutral Axis of B-29 Wing} = 2910 y \text{ (lbs.)}$$

where y is obtained from Tables III-A and III-B.

$$\Delta \text{ Torsional Moment about N.A. of B-29 Wing} = 665 \times 10^3 \alpha \text{ (ft.-lbs.)}$$

where α is obtained from Table III-A and III-B.

When the vertical translation of the B-29 airplane is included in the equations of symmetrical motion, the transient response is not appreciably changed but a slow divergence is indicated. This effect is shown in Figure III-A and III-B. The presence of this divergence implies that hands-off flight is theoretically not feasible with a mechanically actuated single-aileron control and has led to an investigation of a single-point method of attachment employing an automatic pilot type of control.

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Table I

Schedule of Runs #1 - #270

Symmetrical and Anti - Symmetrical Motion

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TABLE I

WING TIP COUPLING PROJECT MX-1016
 SCHEDULE OF RUNS DONE AT O.A.R. DEC. 4, 1950
 ANTI-SYMMETRICAL & SYMMETRICAL MOTION

Run #	Altitude	Speed (ft/sec)	W ₈₄ (#)	W ₂₉ (#)	X	CG ₈₄ Position
1	Sea Level	259	14500	90000	0	.280 MAC
2					1.5	
3					3.0	
4			105000		0	
5					1.5	
6					3.0	
7			120000		0	
8					1.5	
9					3	
10		344		90000	0	
11					1.5	
12					3	
13			105000		0	
14					1.5	
15					3	
16			120000		0	
17					1.5	
18					3	
19		410		90000	0	
20					1.5	
21					3	
22			105000		0	
23					1.5	
24					3	
25			120000		0	
26					1.5	
27					3	
28		259	13000	90000	0	
29					1.5	
30					3	
31			105000		0	
32					1.5	
33					3	
34			120000		0	
35					1.5	
36					3	
37		344		90000	0	
38					1.5	
39					3	
40			105000		0	
41					1.5	
42					3	
43			120000		0	
44					1.5	
45					3	
46		410		90000	0	
47					1.5	
48					3	
49				105000	0	

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Schedule of Runs (continued)

Run #	Altitude	Speed (ft/sec)	$W_{84}(\#)$	$W_{29}(\#)$	K	CG ₈₄ Position
50	Sea Level	410	13000	105000	1.5	.280 MAC
51					3	
52				120000	0	
53					1.5	
54					3	
55		259	11500	90000	0	
56					1.5	
57					3	
58				105000	0	
59					1.5	
60					3	
61				120000	0	
62					1.5	
63					3	
64		344		90000	0	
65					1.5	
66					3	
67				105000	0	
68					1.5	
69					3	
70				120000	0	
71					1.5	
72					3	
73		410		90000	0	
74					1.5	
75					3	
76				105000	0	
77					1.5	
78					3	
79				120000	0	
80					1.5	
81					3	
82	20000	354	14500	90000	0	
83					1.5	
84					3	
85				105000	0	
86					1.5	
87					3	
88				120000	0	
89					1.5	
90					3	
91		434		90000	0	
92					1.5	
93					3	
94				105000	0	
95					1.5	
96					3	
97				120000	0	
98					1.5	
99					3	

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The results shown in Table III-A for symmetric motion were obtained for a four degree of freedom system containing θ , y , β , and α variables [since $\delta = f(y)$], assuming that the influence of w upon the resultant motion was negligible. Subsequent analysis indicated otherwise.

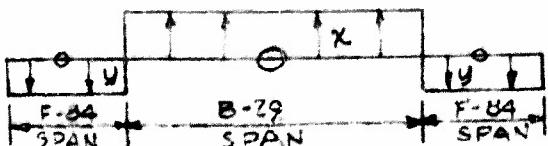
The results shown in Table III-B for anti-symmetric motion were obtained for a four degree of freedom system consisting of θ , y , β , and α variables.

B. Gust Disturbances

The design gust distributions considered in this report consist of vertical gusts having symmetrical and anti-symmetrical components. The motion resulting from a horizontal gust has not been treated here, but is amenable to analytic solution and had been previously computed. Since the equations of motion are linear, the total motion in any variable is the vectorial sum of that caused by the symmetrical gust (Table III-A) and that caused by the anti-symmetrical gust (Table III-B).

The symmetrical gust distribution is:

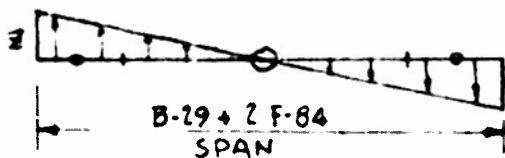
Sparwise:

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where the maximum values of x and y are obtained from the table below:

Altitude	$X_{max.}$	$Y_{max.}$
Sea Level	14.0 ft/sec	7.3 ft/sec
20,000 ft.	17.1 ft/sec	8.9 ft/sec
35,000 ft.	21.0 ft/sec	10.8 ft/sec

The anti-symmetrical gust distribution is:



where the maximum value of Z is obtained from the table below:

Altitude	$Z_{max.}$
Sea Level	6.8 ft/sec
20,000 ft.	9.2 ft/sec
35,000 ft.	12.0 ft/sec

The variation of the gust magnitude, both symmetrical and anti-symmetrical, with time is given by:

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} X_{max.} \\ Y_{max.} \\ Z_{max.} \end{bmatrix} e^{-4.75t} [1 - e^{-5t}]$$

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where $e^{-4.75t} [1 - e^{-0.5t}] = I$, and corresponds to a gust gradient distance of approximately ten B-29 mean aerodynamic chord lengths.

C. Results of Analog Computer Investigation

The maximum values of the resultant oscillations are given in Table III-A for symmetrical motion, and in Table III-B for the anti-symmetrical motion. These values were obtained from the computer records of the 540 runs, a typical one being shown in Figure II-A and Figure II-B for Runs #121, 122, and 123.

The results indicate that single-aileron operation would provide satisfactory and stable motion, and that the effect of increasing K, which is the ratio of aileron deflection , is to reduce the maximum magnitude of the flapping deflection, β .

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Table I

Schedule of Runs #1 - #270

Symmetrical and Anti - Symmetrical Motion

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TABLE I

WING TIP COUPLING PROJECT NY-1016
 SCHEDULE OF RUNS DONE AT O.A.R. DEC. 4, 1950
 ANTI-SYMMETRICAL & SYMMETRICAL MOTION

Run #	Altitude	Speed (ft/sec)	W_{E4} (#)	W_{29} (#)	X	CG _{B4} Position
1	Sea Level	259	14500	90000	0	.280 MAG
2					1.5	
3					3.0	
4				105000	0	
5					1.5	
6					3.0	
7				120000	0	
8					1.5	
9					3	
10		344		90000	0	
11					1.5	
12					3	
13				105000	0	
14					1.5	
15					3	
16				120000	0	
17					1.5	
18					3	
19		410		90000	0	
20					1.5	
21					3	
22				105000	0	
23					1.5	
24					3	
25				120000	0	
26					1.5	
27					3	
28		259	13000	90000	0	
29					1.5	
30					3	
31				105000	0	
32					1.5	
33					3	
34				120000	0	
35					1.5	
36					3	
37		344		90000	0	
38					1.5	
39					3	
40				105000	0	
41					1.5	
42					3	
43				120000	0	
44					1.5	
45					3	
46		410		90000	0	
47					1.5	
48					3	
49				105000	0	

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Schedule of Runs (continued)

Run #	Altitude	Speed (ft/sec)	W ₈₄ (#)	W ₂₉ (#)	K	CG ₈₄ Position
50	Sea Level	410	13000	105000	1.5	.280 MAC
51					3	
52				120000	0	
53					1.5	
54					3	
55		259	11500	90000	0	
56					1.5	
57					3	
58				105000	0	
59					1.5	
60					3	
61				120000	0	
62					1.5	
63					3	
64		344		90000	0	
65					1.5	
66					3	
67				105000	0	
68					1.5	
69					3	
70				120000	0	
71					1.5	
72					3	
73		410		90000	0	
74					1.5	
75					3	
76				105000	0	
77					1.5	
78					3	
79				120000	0	
80					1.5	
81					3	
82	20000	354	14500	90000	0	
83					1.5	
84					3	
85				105000	0	
86					1.5	
87					3	
88				120000	0	
89					1.5	
90					3	
91		434		90000	0	
92					1.5	
93					3	
94				105000	0	
95					1.5	
96					3	
97				120000	0	
98					1.5	
99					3	

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Schedule of Runs (continued)

Run #	Altitude	Speed (ft/sec)	W ₈₄ (#)	W ₂₉ (#)	K	CG ₈₄ Position
100	20000	501	14500	90000	0	.280 MAC
101					1.5	
102					3	
103				105000	0	
104					1.5	
105					3	
106				120000	0	
107					1.5	
108					3	
109		354	13000	90000	0	
110					1.5	
111					3	
112				105000	0	
113					1.5	
114					3	
115				120000	0	
116					1.5	
117					3	
118		434		90000	0	
119					1.5	
120					3	
121				105000	0	
122					1.5	
123					3	
124				120000	0	
125					1.5	
126					3	
127		501		90000	0	
128					1.5	
129					3	
130				105000	0	
131					1.5	
132					3	
133				120000	0	
134					1.5	
135					3	
136	20000	354	11500	90000	0	
137					1.5	
138					3	
139				105000	0	
140					1.5	
141					3	
142				120000	0	
143					1.5	
144					3	
145		434		90000	0	
146					1.5	
147					3	
148				105000	0	
149					1.5	

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Schedule of Runs (continued)

Run #	Altitude	Speed (ft/sec)	W ₈₄ (#)	W ₂₉ (#)	X	CG ₈₄ Position
150	20000	434	11500	105000	3	.280 MAC
151				120000	0	
152					1.5	
153					3	
154		501		90000	0	
155					1.5	
156					3	
157				105000	0	
158					1.5	
159					3	
160				120000	0	
161					1.5	
162					3	
163	35000	465	14500	90000	0	
164					1.5	
165					3	
166				105000	0	
167					1.5	
168					3	
169				120000	0	
170					1.5	
171					3	
172		520		90000	0	
173					1.5	
174					3	
175				105000	0	
176					1.5	
177					3	
178				120000	0	
179					1.5	
180					3	
181		570		90000	0	
182					1.5	
183					3	
184				105000	0	
185					1.5	
186					3	
187				120000	0	
188					1.5	
189					3	
190		465	13000	90000	0	
191					1.5	
192					3	
193				105000	0	
194					1.5	
195					3	
196				120000	0	
197					1.5	
198					3	
199		520		90000	0	

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Schedule of Runs (continued)

Run #	Altitude	Speed (ft/sec)	W ₈₄ (#)	W ₂₉ (#)	K	CG ₈₄ Position
200	35000	320	13000	90000	1.5	.280 MAC
201					3	
202				105000	0	
203					1.5	
204					3	
205				120000	0	
206					1.5	
207					3	
208		570		90000	0	
209					1.5	
210					3	
211				105000	0	
212					1.5	
213					3	
214				120000	0	
215					1.5	
216					3	
217		465	11500	90000	0	
218					1.5	
219					3	
220				105000	0	
221					1.5	
222					3	
223				120000	0	
224					1.5	
225					3	
226		520		90000	0	
227					1.5	
228					3	
229				105000	0	
230					1.5	
231					3	
232				120000	0	
233					1.5	
234					3	
235		570		90000	0	
236					1.5	
237					3	
238				105000	0	
239					1.5	
240					3	
241				12000	0	
242					1.5	
243					3	
244	Sea Level	259	13000	105000	0	.233 MAC
245					1.5	
246					3	
247		344			0	
248					1.5	
249					3	

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TABLE II A-SYMMETRICAL MOTION EQUATIONS.

	ω''	ω'	ω	γ'	γ	θ''	θ'	θ	α''	α'	α	β''	β'
EQUATION 1	$\frac{M+2m}{g \times 10^3} \frac{12.22}{V}$	—	$\frac{3.696m}{g \times 10^3}$	$\frac{5.201}{V}$	—	$\frac{-2m(3.23+q)}{g \times 10^3}$	$\frac{-70.52}{V}$	-12.217	$\frac{-2m\alpha}{g \times 10^3}$	$\frac{-9.88}{V}$	-2.998	$\frac{36.6m}{g \times 10^3}$	47.52
EQUATION 2	$\frac{2m(3.23+q)}{g \times 10^3} \frac{22.02}{V}$	—	$\frac{3.96m(3.23+q)}{g \times 10^3}$	$\frac{20.14}{V}$	—	$\frac{1.72m(3.23+q)}{g \times 10^3}$	$\frac{3275}{V}$	18.64	$\frac{3m(3.23+q)}{g \times 10^3}$	$\frac{213}{V}$	9.38	$\frac{36.6m(3.23+q)}{g \times 10^3}$	198.36
EQUATION 3	$\frac{15.3m}{g \times 10^3} \frac{24.41}{V}$	—	$\frac{m[33.0+0.063]}{g \times 10^3}$	$\frac{44.30}{V}$	—	$\frac{18.3m(3.23+q)}{g \times 10^3}$	$\frac{100}{V}$	-24.36	$\frac{18.3m\alpha}{g \times 10^3}$	$\frac{90.5}{V}$	-22.25	$\frac{m[33.5+0.1]}{g \times 10^3}$	47.54
EQUATION 4	$\frac{m}{g \times 10^3} \frac{1.461}{V}$	—	$\frac{1.848m}{g \times 10^3}$	$\frac{2.269}{V}$	$\frac{2.91}{g}$	$\frac{-m(3.23+q)}{g \times 10^3}$	$\frac{-5.46}{V}$	-1.457	$\frac{m\alpha}{g \times 10^3}$	$\frac{4.94}{V}$	-1.237	$\frac{15.3m}{g \times 10^3}$	22.26
EQUATION 5	—	$\frac{101793-4.09}{V}$	—	—	$\frac{15.6259-6.767}{V}$	$\frac{2.71a}{g}$	$\frac{m\alpha}{g \times 10^3}$	$\frac{9.90}{V}$	$\frac{3.303-10.54}{m\alpha g}$	$\frac{89.7}{g \times 10^3}$	$\frac{4.65+2.896}{V}$	-6.5268	$103.8-66.35$

ϕ FORCING FUNCTION

EQUATION 1	$1.0886+1.622K \frac{[25.11x-76.98]}{V}$	X
EQUATION 2	$\frac{[6.086+1.536K]}{V} \frac{[39.74-284.5x]}{V}$	X
EQUATION 3	$\frac{1.4402+2.63K}{V} \frac{[68.51-562.5x]}{V}$	X
EQUATION 4	$\frac{0.0779+0.084K}{V} \frac{[6.05x-31.35x]}{V}$	X
EQUATION 5	$\frac{[5.86+6.22K]}{V} \frac{[34.2x+13.98x]}{V}$	X

M = MASS OF F-84, SLUGS.
 Q = DYNAMIC PRESSURE, LB./SQ.FT.
 V = VELOCITY, FT./SEC.
 R = RADIUS OF GYRATION IN ROLL OF F-84, FT.
 C_a = DISTANCE FROM E.A. OF B-29 WING TO C.G. OF F-84, FT.
 C_g = CENTER OF GRAVITY POSITION OF F-84, FT.
 K = AUTOMATIC AILERON DRIVE RATIO.
 R_g = RADIUS OF GYRATION IN PITCH OF F-84, FT.
 M = MASS OF B-29 AIRPLANE, SLUGS.
 X = MAX. VALUE OF PITCH DISTURBANCE OVER B-29, FT./SEC.
 y = MAX. VALUE OF PITCH DISTURBANCE OVER F-84, FT./SEC.
 $I_{z,z}$ = PITCH MOMENT OF INERTIA OF B-29, SLUGS-(FT).

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Schedule of Runs (continued)

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Run #	Altitude	Speed (ft/sec)	W ₈₄ (#)	W ₂₉ (#)	K	CG ₈₄ Position
250	Sea Level	410	13000	105000	0	.233 MAC
251					1.5	
252					3	
253	20000	354			0	
254					1.5	
255					3	
256		434			0	
257					1.5	
258					3	
259		501			0	
260					1.5	
261					3	
262	35000	465			0	
263					1.5	
264					3	
265		520			0	
266					1.5	
267					3	
268		570			0	
269					1.5	
270					3	

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TABLE II B—ANTI-SYMMETRICAL MOTION EQUATIONS.

	$\ddot{\phi}$	$\dot{\phi}$	ϕ	y'	y	α'	α	β'	β
EQUATION 1	$\frac{I_{xx} + 2m[640 + k]}{g \times 10^3}$	494.40	\sqrt{V}	$\frac{2m[657.0443]}{g \times 10^3}$	598.6	$\frac{179.2ma}{g \times 10^3}$	$-\frac{885}{V}$	-221.0	$\frac{814.9}{g \times 10^3}$
EQUATION 2	$m[640 + k]$	177.9	\sqrt{V}	$m[33.8 + 0.443k]$	44.30	$\frac{-18.3ma}{g \times 10^3}$	$-\frac{90.5}{V}$	-22.25	$\frac{475.4}{g \times 10^3}$
EQUATION 3	$89.6m$	100.50	\sqrt{V}	$\frac{1.848m}{g \times 10^3}$	2.269	$\frac{ma}{g \times 10^3}$	$-\frac{4.94}{V}$	-1.237	$\frac{18.3m}{g \times 10^3}$
EQUATION 4	$687cg - 309.6$	\sqrt{V}	\sqrt{V}	$15.62cg - 6.757$	$2.91a$	$\frac{m k_x^2}{g \times 10^3}$	$\frac{89.7}{V}$	$\frac{665}{g} + 2.896$	$\frac{22.26}{-8.52cg}$

β Force Function

EQUATION 1	$13.91 + 17.25k$	$\frac{8635Z}{\sqrt{V}} X$
EQUATION 2	$1.402 + 2.63k$	$\frac{483Z}{\sqrt{V}} X$
EQUATION 3	$.0779 + .0844k$	$\frac{27.28Z}{\sqrt{V}} X$
EQUATION 4	$\frac{[536 + .622k]g}{-[230 + 155k]}$	$\frac{12.16Z}{\sqrt{V}} X$

I_{xx} = ROLL MOMENT OF INERTIA OF B-29, SLUGS-FT.².

m = MASS OF F-84, SLUGS.

q = DYNAMIC PRESSURE, LB/SQ.FT.

V = VELOCITY, FT/SEC.

k_x = RADIUS OF GYRATION IN ROLL OF F-84, FT.

Q = DISTANCE FROM E.A. OF B-29 WING TO C.G. OF F-84, FT.

C.G. = CENTER OF GRAVITY POSITION OF F-84, FRACTION OF M.A.C.

K = AUTOMATIC AILERON DRIVE RATIO.

$\frac{k_x}{Z}$ = RADIUS OF GYRATION IN PITCH OF F-84, FT

Z = MAX. VALUE OF ROLL DISTURBANCE VELOCITY, FT./SEC.

CONTINUED

TABLE II-C.MASS AND INERTIA CHARACTERISTICS.

	F-84 AIRPLANE.			B-29 AIRPLANE.		
WEIGHT. (LBS.)	14500	13000	11500	120000	105000	90000
MASS. (SLUGS)	450	404	357	3728	3260	2795
I_{x-x} FT.	5.88	5.85	5.48			
I_{y-y} FT.	6.11	6.16	6.50			
I_{x-x} (SLUGS-FT ²)				1712×10^3	1500×10^3	1285×10^3
I_{y-y} (SLUGS-FT ²)				1000×10^3	875×10^3	750×10^3

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TABLE II-D

COEFFICIENTS OF EQUATIONS OF MOTION

SYMMETRICAL AND ANTI-SYMMETRICAL MOTION

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	W&A	CG-2	W-29	CG-3
PREPARED				
CHEESED				
REVISED				
WEIGHTS	14,500 lbs.	90,000 lbs.		
ALTITUDE				
TIME				

EDB-0905-104

CONTINUE

COEFFICIENTS OF EQUATIONS OF MOTION

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION RUNS 1, 2, 3																				
SYNTHETIC MOTION																				
α_{xx}	α_{yy}	α_{zz}	β_{xx}	β_{yy}	β_{zz}	θ_{xx}	θ_{yy}	θ_{zz}	α_x	α_y	α_z	β_x	β_y	β_z	θ_x	θ_y	θ_z	α_{xx}	α_{yy}	α_{zz}
.07619	.07278	-	.02079	.02008	-	.03321	.27223	.12.217	.001969	.03715	.2.298	.2050	.1935	.15338	.4.711	.56324	.-11.411			
-1.03531	.06502	-	.07079	.07776	-	.9.925	.12.64	.18.64	.4.265	.0.3224	.9.38	-.7011	-.7659	-.6860	.1.490	.2.294	.-8.622	X		
.1029	.09225	-	.1991	.1770	-	-.3505	-.3861	.21.36	.01211	-.3124	-.22.25	2.079	1.826	1.402	.5.347	.9.292	.12.698			
.005625	.005641	-	.01039	.005741	.03537	-.01.915	-.02.018	.-1.457	.00009544	-.01.907	-.1.237	.1.729	.03295	.07779	.2021	.3.302	.5.566	X		
-	-.004797	-	-	-.006202	.005966	.21.00	.3822	.4.610	.0.2100	.0.3653	.8.823	-	-.09077	-.07992	-.05118	-.02224	.4.673	X		
ANTI-CYCLOTRON MOTION																				
ϕ_{xx}	ϕ_{yy}	ϕ_{zz}	ψ_{xx}	ψ_{yy}	ψ_{zz}	χ_{xx}	χ_{yy}	χ_{zz}	α_x	α_y	α_z	β_x	β_y	β_z	θ_x	θ_y	θ_z	α_{xx}	α_{yy}	α_{zz}
106.5	190.9	-	1.82	2.311	-	-.1764	-.3.417	-.221.0	16.35	31.76	13.27	39.79	65.66	276.7X						
244.9	6.869	-	.1991	.2216	-	.01.021	-.3.326	-.22.25	2.079	1.736	1.402	.5.317	.9.292	.12.673						
504.0	.33920	-	.11.029	.04.7261	.02337	.20009544	-.01.907	-.1.337	.1.059	.6.125	.1.719	.8.2941	.1.202	.7.167X						
-	-.4527	-	-	-.009262	.00.366	.21.0	.0.413	.0.23	-	-.09771	-.07992	-.01118	-.00774	-.2103X						

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PREPARED _____
CHECKED _____
REVISED _____

$$\text{Alt.} = \text{Sea Level}$$

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VFT/Sec = 259

TABLE II
COEFFICIENTS OF EQUATIONS OF MOTION
RUNS # 4, 5, 6

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION RUNS # 4, 5, 6																					
SYNTHETIC MOTION																					
ANTI-SYNT. MOTION																					
	ω'	ω	ω''	ϕ'	ϕ	ϕ''	θ'	θ	θ''	α'	α	α''	β'	β	β''	$K=0$	$K=1.5$	$K=3.0$	$K=0$	$K=1.5$	$K=3.0$
1	.05200	.04718	-	.02079	.03003	-	.03831	-	.031960	-.028115	2.90	-.2019	.1935	.1038	.4411	.6934	.11.41	X			
2	-.03331	-.05502	-	-.07079	-.07776	-	11.40	12.64	18.64	1.267	.0224	9.38	-.7611	-.7459	-.6.60	-.1.490	-.6.62	X			
3	1.029	.09225	-	.1291	.1710	-	.2505	-.2601	-.24.36	-.01.01	-.3494	-.22.25	2.079	1.436	1.402	5.347	9.292	12.691			
4	.005685	.007641	-	.01039	.03576	.03577	-.01125	-.02105	-.02105	-.000324	-.01.907	-.1.237	.1029	.06595	.0779	.3041	.3392	.5563			
5	-	-.004797	-	-	-.007292	.003366	.2100	.3522	.4610	.2100	.3463	3.323	-	-.09077	-.07952	-.05116	-.0.224	-.46.33			
	Φ'	Φ	Φ''	ψ'	ψ	ψ''	α'	α	α''	β'	β	β''	$K=0$	$K=1.5$	$K=3.0$	Φ'	Φ	Φ''	β'	β	β''
1	100.1	110.2	-	1.352	2.211	-	-1764	-2.417	-221.0	13.35	31.46	13.51	32.72	15.66	22.67	X					
2	9.419	6.060	-	.1971	.1710	-	-.01501	-.01501	-.3294	-22.25	2.079	1.36	1.402	5.347	9.292	12.691					
3	.5040	.3850	-	.01039	.008763	.03537	-.000324	-.01.907	-.1.237	.1029	.04505	.0779	.3041	.3392	.3762	X					
4	-	-.1527	-	-	-.33.2292	.006366	.2100	.3463	.3.323	-	-.09077	-.07952	-.05116	-.0.224	-.46.33						

ALTITUDE = Sea Level
 $\frac{W34}{W29} = 14500\text{ft}$
 $\frac{W29}{W29} = 120000\text{ft}$

REF ID: A6512

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II - D COEFFICIENTS OF EQUATIONS OF MOTION RINGS * 7 & 9																				
SYMMETRIC MOTION																				
ω ω' ω'' θ θ' θ'' α α' α'' β β' β'' ρ ρ' ρ'' θ θ' θ'' ρ ρ' ρ''																				
.05785	.04718	-	.02039	.02031	-	.03831	.2723	12.217	-.001969	.03615	2.993	.20359	.1335	.1638	.4411	.6924	-.11.413			
-.02331	.00502	-	-.07079	-.07776	-	13.05	12.64	18.64	.0267	.0224	9.38	-.7011	-.7659	-.6360	-.1490	-.2274	.0.6221			
.1039	.09435	-	.1991	.1710	-	.3595	-.3861	-24.36	-.01801	-.3494	-22.25	2.079	1.636	1.402	5.347	9.292	12.671			
.005625	.005621	-	.01039	.008761	.03637	-.01.915	-.02108	-.1.457	-.0007644	-.01907	-.1.237	.1029	.08295	.0779	.2041	.2302	.56661			
-.004797	-	-	-.009209	.0066366	.2100	.3822	.4610	.2100			.3463	.6.623	-	-.09077	-.07992	-.05113	-.02244	-.46431		
ANTI-SYMMETRIC MOTION																				
ϕ ϕ' ϕ'' ψ ψ' ψ'' α α' α'' β β' β'' ρ ρ' ρ'' θ θ' θ'' ρ ρ' ρ''																				
111.3	190.2	-	1.882	2.711	-	-.174	-.3.417	-.221.0	18.85	31.46	13.21	29.77	65.66	226.7						
2.419	6.869	-	.1991	.1710	-	-.01631	-.02694	-.22.25	2.079	1.736	1.402	5.247	9.292	12.66						
.5040	.3830	-	.01039	.008761	.03637	-.0009844	-.01907	-.1.237	.1029	.08295	.0779	.2041	.3302	.7162						
-.1527	-	-	-.009202	.0066366	.2100	.3463	.8.623	-		-.09077	-.07992	-.05113	.02244	-.3193						

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CHECKED
REVISED

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Alt. = Sea Level
 $V_{A1} = 14500\text{ft}$
 $V_{A2} = 9000\text{ft}$
 $H_{20} = 3160.45 \pm .175 \text{ ft.}$

$V_{A1}/\text{sec} = 344$
 $C.G. \alpha_4 = .260$

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----

TABLE II - D
COEFFICIENTS OF EQUATIONS OF MOTION
RUNS #10, 11, 12

STRUCTURE MOTION

θ'	θ	θ''	θ'''	$\theta^{(4)}$	$\theta^{(5)}$	$\theta^{(6)}$	$\theta^{(7)}$	$\theta^{(8)}$	$\theta^{(9)}$	$\theta^{(10)}$	$\theta^{(11)}$	$\theta^{(12)}$	$\theta^{(13)}$	$\theta^{(14)}$	$\theta^{(15)}$	$\theta^{(16)}$	$\theta^{(17)}$	$\theta^{(18)}$	$\theta^{(19)}$
Eq. 1. 0.06339	.03552	-	.01136	.03512	-	-0.02139	.02050	-12.217	-0.01125	-0.02872	-2.998	.1176	.1381	.1411	.1411	.6234	.8.587	X	
2. -.02159	-.06401	-	-.00465	-.05855	-	5.671	2.230	16.64	2.238	61.92	9.380	-1.004	-57.66	-66.60	-1.490	-2.294	6.492	X	
3. 0.05882	.07096	-	.1133	.1288	-	-2.003	-.2907	-24.26	-.01029	-.2631	-26.25	1.138	1.332	1.402	5.247	9.292	9.554	X	
4. 0.00224	.00247	-	.002940	.0065936	.020779	-.01094	-.01537	-1.457	-.0005625	-.01436	-1.237	.05632	.06471	.0779	.2011	.3302	.4191	X	
5. -	-.003612	-	-	-.006528	.003637	.1200	.2378	.4610	.1200	.2608	.5.260	-	-.06334	-.07992	-.07116	-.02244	-.3496	X	

ANTI-SYM MOTION

θ'	θ	θ''	θ'''	$\theta^{(4)}$	$\theta^{(5)}$	$\theta^{(6)}$	$\theta^{(7)}$	$\theta^{(8)}$	$\theta^{(9)}$	$\theta^{(10)}$	$\theta^{(11)}$	$\theta^{(12)}$	$\theta^{(13)}$	$\theta^{(14)}$	$\theta^{(15)}$	$\theta^{(16)}$	$\theta^{(17)}$	$\theta^{(18)}$	$\theta^{(19)}$
Eq. 1. 60.66	143.7	-	1.075	1.720	-	-1.068	2.573	-22.0	10.77	23.6	12.91	39.79	65.66	170.7	-	-	-	-	-
2. 5.383	5.172	-	.1138	.1288	-	-.01029	-.2631	-22.25	1.128	1.382	1.402	5.347	9.292	9.547	-	-	-	-	-
3. 2.293	.2922	-	.003940	.0065936	.020779	-.0005625	-.01436	-1.237	.05632	.06471	.0779	.2011	.3302	.4191	-.5392	X	-	-	-
4. -	-.3495	-	-	-.006528	.003637	.1200	.2608	.5.260	-	-.06334	-.07992	-.07113	-.02244	-.3496	X	-	-	-	-

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Alt. = Sea Level
 W₄ = 14500#
 W₂₉ = 105000#
 q = 5140.05 .175 Ft.
 C.G. = .280

V_T/sec = 344
 REPORT NO. 26-0905-104
 DATE 10-19-48
 MOLEL

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
--	---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----

TABLE II-D
COEFFICIENTS OF EQUATIONS OF MOTION

STATIONARY MOTION

	ψ''	ψ'	ψ	ψ''	θ'	θ	α'	α	β''	β'	α	β''	β'	α	β''	β'	α	β''	β'	α
No. 1	.03572	.03552	-	.01188	.01512	-	-.02139	-.02050	-.12-217	-.00116	-.02872	-.2-998	-.1176	1.361	.1858	.441	.692	3.587	X	
2	-.02189	-.06401	-	-.04045	-.05835	-	6.566	9.520	18.64	.2438	.6192	9.380	-.5766	-.6360	-.4004	-.1490	-.2-294	6.492	X	
3	.05832	.07096	-	.2436	.1288	-	-.2003	-.2507	-.24.36	-.01029	-.2631	-.22.25	1.163	1.382	1.402	5.347	9.292	9.554	X	
4	.005214	.006247	-	.005240	.006596	.02079	-.01094	-.01587	-.1.457	-.0005635	-.01126	-.1.237	.05882	.06471	.0779	.2041	.3302	.4191	X	
5	-	.003612	-	-	-.006928	.003697	.1200	.28778	.4610	.1200	.2608	.5260	-	-.06324	-.07992	-.05118	-.02244	-.34968	-	

ANTI-SYMMETRIC MOTION

	ϕ''	ϕ'	ϕ	ϕ''	θ'	θ	α'	α	β''	β'	α									
No. 1	62.36	143.7	-	1.075	1.740	-	-.1008	-.2573	-.221.0	10.77	23.69	13.71	39.70	65.66	170.7	X				
2	5.363	5.172	-	.1138	.1288	-	-.01029	-.2631	-.22.25	1.188	1.382	1.402	5.347	9.292	9.554	X				
3	28.30	.2922	-	.005940	.006596	.02079	-.0005635	-.01436	-.01.237	.05882	.06471	.0779	.2041	.3302	.4191	X				
4	-	.3406	-	-	-.006928	.003697	.1200	.2608	.5260	-	-.06324	-.07992	-.05118	-.02244	-.34968	-				

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Alt.	Sea Level	V ft/sec	410
#84	= 14,500 ft	= .84	= .175 ft.
#29	= 90,000 ft	= 0.84	= .280
g	= 200		

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COEFFICIENTS OF EQUATIONS OF MOTION.

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Date 29
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Alt. = Sea Level
WB4 = 14,500 ft. 140
R29 = 105,000 ft. .175 ft.
q = 200 .0884 .280

PREPARED _____
CHECKED _____
REVIEWED _____



	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

TABLE II - D
COEFFICIENTS OF EQUATIONS OF MOTION.
RUNS # 22, 23, 24.

	SYNTHETIC MOTION										ANTI-SYNTHETIC MOTION									
	ω'	ω''	α'	α''	θ'	θ''	β'	β''	γ'	γ''	κ'	κ''	λ'	λ''	μ'	μ''	ν'	ν''	ρ'	ρ''
Eq. 1	.02080	.02980	.008316	.01269	-.01532	-.1720	-12.217	-.0007876	-.02210	-2.298	.08236	.1159	.1888	.4411	.6934	.7208X				
2	.01532	.05371	.02832	-.04922	4.506	7.988	18.64	.1707	.5195	9.38	-.2804	-.4438	-.6860	-.1490	-.2294	5.447X				
3	.04116	.05954	.07964	.1080	.26.02	-.24.39	-24.36	.00724	-.2237	-22.25	.83316	1.160	1.402	5.347	9.42X	8.016X				
4	.002250	.003563	.004156	.005534	.01255	-.007660	-.01332	-.1457	-.0003938	-.01205	-.1.237	.04116	.05429	.0779	.2441	.3302	.3516X			
5	.001030		-.005813	.002546	.08600	.2435	.4610	.08400	.2188	3.835	-.05734	-.07992	-.05118	-.02244	-.2933X					

(Eq. 1
2
3
4
5)

80 80 80

$$\frac{Vft/sec}{C.G. ft} = \frac{259}{.280} = 925$$

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卷之三

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21

COEFFICIENTS OF EQUATIONS OF MOTION	SIMMETRIC MOTION	RUNS #
		31,32-33

	\bar{w}	\bar{v}	\bar{u}	\bar{x}	\bar{y}	\bar{z}	\bar{g}	$\bar{\theta}$	$\bar{\phi}$	$\bar{\psi}$	\bar{P}
Eq 1	.05085	.047218	--	.01866	.02006	--	-.03439	-.2723	-12.217	-.691757	-.03815
2	-.03439	-.08542	--	.06352	-.07776	--	11.44	12.64	18.64	.8221	9.35
3	.05021	-.09125	--	1282	1710	--	-.3148	-.3861	-.2136	-.01617	-.3491
4	.005050	.015641	--	.009332	.008761	.036317	-.01720	-.021048	-.01457	-.0008837	-.01907
5	--	-.04727	--	.009202	.006366	.1916	.3822	.610	.1916	.36163	8.823

ANTENNAE

PREPARED G. M. 8-31-50
CHEKED _____
REVISED _____

Alt.	Sea Level
84	13000 #
84	12000 #
29	80. a. a. J.

$$\frac{V_{\text{fl}}}{m_{\text{so}}} = 259$$

$$C.G. \cdot z = .280$$

EDR-C905-10

CONFIDENTIAL

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION. RUNS # 34, 35, 36																					
SYMMETRIC MOTION																					
K = 0 K = 3.5 K = 3																					
	θ'	θ''	x'	y'	θ'''	θ''''	x''	y''	θ'''''	θ''''''	x''''	y''''	θ'''''''	θ''''''''	x''''''	y''''''	θ''''''''	θ'''''''''	x'''''''	y'''''''	
1	.05670	.04718	.02008	--	-.03439	-.2973	-.12.217	-.001767	-.00315	-.2.998	1.618	1.888	.1835	.6934	.6411	.6934	-.11.11				
2	-.03639	-.08502	-.06354	-.07776	--	13.90	12.64	18.64	3.693	2.8216	2.318	-6.222	-7.659	-1.866	-1.230	-2.236	5.652				
3	.09245	--	.17572	.17120	--	2.3248	-3.8821	-24.36	-.01617	-.31926	.922.25	1.865	1.836	1.1602	5.347	9.292	12.69				
4	.00550	.005671	--	.003332	.005761	.03637	-.01720	-.02108	-.1.657	-.00026831	-.01207	-.1.237	.08525	.0773	.2043	.3302	.5566				
5	--	-.004777	--	--	-.0039202	.004366	.1916	.3822	.1916	.1916	.3463	.3.823	--	-.09007	-.07302	-.05118	-.02244	-.1643			
ANTI-SYMMETRIC MOTION																					
	θ'	θ''	x'	y'	θ'''	θ''''	x''	y''	θ'''''	θ''''''	x''''	y''''	θ'''''''	θ''''''''	x'''''''	y'''''''	θ''''''''	θ'''''''''	x'''''''	y'''''''	
1	102.5	130.9	--	1.630	2.231	--	-2.554	-.3.637	-.221.0	116.32	11.21	33.59	65.66	226.7							
2	2.452	6.869	--	1727	.1720	--	-.01t.7	-.2.924	-.22.25	1.865	1.836	1.602	5.347	9.292	12.69						
3	.5825	.3880	--	0.332	.6761	.03637	-.00026831	-.01907	-.1.237	.03211	.08525	.0773	.2043	.3302	.5566	.7162					
4	--	-.1527	--	--	-.0039202	.004366	.1916	.3822	.1916	.3.823	--	-.09007	-.07302	-.05118	-.02244	-.3193					

1

CONFIDENTIAL

PREPARED R. M. DUNLOP
CHECKED _____
REVISED _____

Alt. = Sea Level
W₈₄ = 13000 ft.
W₂₉ = 90000 ft.
q = 140, a = .175 ft.

PLATE 34
Wt./sec = 344
C.G. = 280
CONFIDENTIAL - REF ID: A204965-104

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
--	---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----

COEFFICIENTS OF EQUATIONS OF MOTION.

TABLE II-D
SYNTHETIC MOTION.

RJMS # 37 39 39

	θ'	v''	v'	v	θ''	θ'	θ	$\dot{\theta}''$	$\dot{\theta}'$	$\dot{\theta}$	$\ddot{\theta}''$	$\ddot{\theta}'$	$\ddot{\theta}$	\ddot{v}''	\ddot{v}'	\ddot{v}	$\ddot{\theta}''$	$\ddot{\theta}'$	$\ddot{\theta}$	
Eq. 1	.02576	.02552	--	.01612	.01612	--	.01365	-.2050	.22317	-.001010	.02872	-.2198	.2056	.1392	.1898	.1411	.6934	-.21567		
2	-.01465	-.01640	--	-.01631	-.01631	--	5.643	9.520	18.64	.2225	.6192	9.380	-.3595	-.5786	-.6360	-.1490	-2.294	6.102		
3	.05281	.05236	--	.01221	.01221	--	.1729	-.2067	.2636	-.003240	-.2632	.2225	.1.066	.1.352	.1.402	.5.267	9.232	9.554		
4	.002886	.004247	--	.003333	.003333	--	.006536	.0079	-.00729	-.01587	-.01457	-.0005050	-.0136	.02337	.02821	.046721	.0779	.2041	.1.191	
5	--	--	--	.006328	.006328	--	.003637	.0095	.2878	.4610	.1095	.2608	.5.260	--	--	-.006324	-.07392	-.05118	-.02214	-.3.964

4. INT. - SYNTHETIC MOTION

	θ'	$\dot{\theta}$	v''	v'	v	$\dot{\theta}''$	$\dot{\theta}'$	$\dot{\theta}$	$\ddot{\theta}''$	$\ddot{\theta}'$	$\ddot{\theta}$					
Eq. 1	55.55	263.7	--	.3657	1.740	--	-.000521	-.21573	-.221.0	2.669	23.69	13.91	39.73	65.66	170.7	
2	4.831	5.172	--	.1221	.1228	--	-.009240	-.2631	-.22.25	1.006	1.382	1.402	5.347	9.232	9.567	
3	2.386	2.382	--	.003333	.006536	.02479	-.0005050	-.01436	-.1.237	.03281	.06471	.0779	.2041	.3302	.5332	
4	--	-.1408	--	--	-.30628	.002637	.0095	.2608	.5.260	--	-.06834	-.07992	-.05118	-.02214	-.2160	

PREPARED G. M. 8-31-50
CHECKED _____
REVISED _____

Alt.	= Sea Level
W84	= 13000 #
W29	= 120000 #
q	= 140, a =

$$\frac{V_{Tc}}{V_{000}} = \frac{34}{84} = \frac{2}{3}$$

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TABLE II-D
COEFFICIENTS OF EQUATIONS OF MOTION
RUNS # 43, 44, 45

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION RUNS # 43, 44, 45																					
SYMMETRIC MOTION																					
$\alpha = 0$ $\alpha = 1.5$ $\alpha = 3.0$																					
	θ^1	θ^2	θ^3	θ^4	θ^5	θ^6	θ^7	θ^8	θ^9	θ^{10}	θ^{11}	θ^{12}	θ^{13}	θ^{14}	θ^{15}	θ^{16}	θ^{17}	θ^{18}	θ^{19}	θ^{20}	θ^{21}
Eq. 1	.03240	.03552	--	.01066	.01512	--	.01965	-.2050	-.12.217	-.001010	-.02872	-2.998	.1056	.1381	.11888	.4411	.6934	.8.587	X		
2	-.01964	-.06401	--	-.01631	-.05835	--	7.429	.2.520	.18.64	.2225	.6192	.9.380	-.3595	-.5766	-.6860	-.1.490	-.2.294	6.162	X		
3	.05281	.07096	--	.1021	.12688	--	-.1799	-.2.997	-.24.36	-.009240	-.2.2631	-.22.25	1.066	1.382	1.402	5.347	9.292	9.551	X		
4	.0028356	.0012217	--	.0053333	.006596	.002079	-.008292	-.01587	-.1.457	-.0005050	-.01136	-.1.237	.02831	.06471	.07729	.2041	.3302	.4191	X		
5	--	-.0031612	--	--	-.0065248	.0031637	.01695	.2878	.4610	.1095	.2608	.5.260	--	--	--	-.06834	-.07992	-.05118	-.02244	-.3436	
ANTI-SYMMETRIC MOTION																					
	θ^1	θ^2	θ^3	θ^4	θ^5	θ^6	θ^7	θ^8	θ^9	θ^{10}	θ^{11}	θ^{12}	θ^{13}	θ^{14}	θ^{15}	θ^{16}	θ^{17}	θ^{18}	θ^{19}	θ^{20}	θ^{21}
Eq. 1	58.57	143.7	--	3657	2.740	--	-.09051	-.2.573	-.221.0	2.669	23.69	13.91	32.79	65.66	170.7	X					
2	4.833	5.172	--	.1021	.12888	--	.009240	-.2.631	-.2.22.25	1.066	1.382	1.402	5.347	9.292	9.551	X					
3	2.586	.2922	--	.0053333	.006596	.002079	-.0005050	-.01136	-.1.237	.05281	.06471	.07729	.2041	.3302	.4191	X					
4	--	.313.08	--	--	-.0065248	.0031637	.01695	.2608	.5.260	--	-.06834	-.07992	-.05118	-.02244	-.3436	X					

(CONFIDENTIAL)

PREPARED G. M. 9-1-50
C.A.C.F.D.
REVISED

Alt. = Sea Level

$\frac{q}{B_L}$ = 15000 ft
 $\frac{q}{B_L}$ = 90000 ft
 $\frac{q}{B_L}$ = 200, a = .175 ft.



CONFIDENTIAL NO. EDR-905-104

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		COEFFICIENTS OF EQUATIONS OF MOTION										COEFFICIENTS OF EQUATIONS OF MOTION																
		RUNS # 46, 47, 48										RUNS # 46, 47, 48																
		<u>B'</u>	<u>B</u>	<u>R'</u>	<u>R</u>	<u>θ'</u>	<u>θ</u>	<u>\dot{x}'</u>	<u>\dot{x}</u>	<u>$\dot{\theta}'$</u>	<u>$\dot{\theta}$</u>	<u>B'</u>	<u>B</u>	<u>θ'</u>	<u>θ</u>	<u>\dot{x}'</u>	<u>\dot{x}</u>	<u>$\dot{\theta}'$</u>	<u>$\dot{\theta}$</u>	<u>B'</u>	<u>B</u>	<u>θ'</u>	<u>θ</u>	<u>\dot{x}'</u>	<u>\dot{x}</u>	<u>$\dot{\theta}'$</u>	<u>$\dot{\theta}$</u>	
Eq. 1	1	.01802	.02380	--	.00164	.01269	--	-.01376	-.1720	-12.217	-.0002068	-.02110	2.998	.07332	.1159	.1888	.4411	.6934	.7208	X								
2	2	-.01376	-.01377	--	-.02562	-.01912	--	3.950	7.988	18.64	.1557	.5195	9.38	-.2517	-.4538	-.6860	-.1430	-.2394	-.4447	X								
3	3	.03656	.03954	--	.02118	.00820	--	-.1259	-.2439	24.36	-.006468	-.2207	.22.25	.7460	1.160	1.402	5.347	9.292	8.016	X								
4	4	.002020	.003563	--	.0033733	.0055376	--	.01655	-.0068880	-.01332	-.16657	-.0003533	-.01205	1.237	.03636	.05129	.07779	.2041	.33102	.35116	X							
5	5	--	-.003030	--	--	-.005813	.002546	.07666	.2615	.4610	.07664	.07664	.2188	3.835	--	--	-.05734	-.07922	-.05118	-.02211	-.23334	X						
A N T I - S Y M M E T R I C MOTION																												
Eq. 1																												
Eq. 2																												
Eq. 3																												
Eq. 4																												

CONFIDENTIAL

REPAIRED _____
CHECKED _____
REVISED _____

Alt. = Sea Level

$$\sqrt{V^2t/\sec} = 410 - \\ C.G. \frac{.280}{84}$$

38
DR-C 905-104

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1000

$$c = 410 - \\ \pi .280$$

C.

Alt. 84 Sea Level
13000 ft.
105000 ft.

9-1-50

RELEASED
CENSORED
BY 115150

49045 NO. EDR-C 905-104

A HISTORY OF THE AMERICAN PEOPLE

$$\frac{V_{ft}}{\sec} = 410 - \\ C.G. \quad \equiv .280 - \\ 84$$

Alt. 84 Sea L 13000
W 29 105000

92-1-50

PREPARED
CHECKED
REVISED

卷之三

TABLE II-D
COEFFICIENTS OF EQUATIONS OF MOTION
RUNS # 4950, 51

SYMMETRIC MOTION

Eq. 1 2 3 4 5

159 221.0 6.768 19.88 13.91 39.72 65.66

Q =	1	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	
1	39.96	120.6	—	6760	1,460	—	-.06336	-2.159	221.0	6.768	19.88	13.91	39.79	65.66	143.2	I				
2	1.382	1.332	—	07248	.0980	—	-.006468	-2207	-22.25	17460	1.160	1.402	5.347	9.292	8.010	I				
3	1810	2451	—	.003733	.005234	.01455	-.0003535	-.01205	-1.237	.03696	.05429	.0779	.2041	.3302	.4524	I				
4	—	-2.363	—	—	-.005813	.002566	.07664	.2188	.835	—	-.05734	-.07792	-.05118	-.02244	-.20174					

Q. 1 2 3 4

REPAIRED 8-11-50 9-2-50
CHECKED _____
REVISED _____

Alt. = Sea Level
 84 = 13000 ft
 29 = 120000 ft
 200, a =

$$\frac{M\pi}{360} = .280$$

CONFIDENTIAL **PAGE 6** **EDR-6905-104**

CONFIDENTIAL

PREPARED _____
 CHECKED _____
 REVISED _____

Alt. = Sea Level
 q = 84 = 11500 ft.
 q = 29 = 90000 ft.
 q = 80, a = .175 ft.



Alt. = 40
 Vrt/sec = 259
 C.G. = .84
 a = .280

Alt. = 40
 Vrt/sec = 259
 C.G. = .84
 a = .280

CONFIDENTIAL

C. J	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF EQUATIONS OF MOTION.																					
SYMMETRIC MOTION																					
RUNS # 55, 56, 57																					
$\alpha = 0 \quad \alpha = 1.5 \quad \alpha = 3.0$																					
	θ^*	θ'	θ''	φ^*	φ'	φ''	ψ^*	ψ'	ψ''	α^*	α'	α''	β^*	β'	β''	γ^*	γ'	γ''	δ^*	δ'	
Eq. 1	.0138	.0272	--	.0165	.0203	--	.0104	.0273	.01217	-.01116	.01382	.01338	.01333	.01835	.01888	.01111	.01111	.01111	.01111	.01111	
2	-.0304	-.0850	--	-.0562	-.0771	--	-.81	.12.64	.18.64	.38.24	.8224	.938	-.5560	-.7659	.0860	-.1.90	-.2.90	-.8.622	-.8.622	-.8.622	
3	.0817	.0943	--	.1570	.1710	--	.24.36	.38.61	.42.36	-.0213	.34.24	.22.25	1.629	1.836	1.836	1.347	1.347	1.347	1.347	1.347	
4	.0045	.0056	--	.0082	.0088	--	.0042	.0032	.0032	-.0032	.0032	.0032	-.0237	-.0237	.0017	.0017	.0017	.0017	.0017	.0017	
5	--	-.0048	--	--	-.0092	--	.0064	.1885	.3822	.4610	.1885	.3822	.8.823	—	-.0908	-.0908	-.0908	-.0908	-.0908	-.0908	

ANTI-SYMMETRIC MOTION

C. J	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
ANTI-SYMMETRIC MOTION																					
$\alpha = 0 \quad \alpha = 1.5 \quad \alpha = 3.0$																					
	θ^*	θ'	θ''	φ^*	φ'	φ''	ψ^*	ψ'	ψ''	α^*	α'	α''	β^*	β'	β''	γ^*	γ'	γ''	δ^*	δ'	
Eq. 1	87.73	190.9	--	169.1	2.311	--	-1.399	-3.417	-2.21.0	1.6.91	31.46	13.91	39.79	65.66	29.67	—	—	—	—	—	
2	7.653	6.869	--	.1570	.1710	--	-.0143	-.3436	-.22.25	1.623	1.836	1.602	5.347	9.232	12.68	—	—	—	—	—	
3	3.998	3.880	--	.0082	.0088	--	-.0098	-.0191	-.1.237	.0817	.0860	.0779	.2041	.3302	.716	—	—	—	—	—	
4	--	-.527	--	--	-.0092	.0064	.1885	.3822	.4610	.1885	.3822	—	-.0908	-.0908	-.0908	-.0908	-.0908	-.0908	-.0908	-.0908	

CONFIDENTIAL

PREPARED 1-14 35-50
CHECKED _____
REVISED _____

Alt. = Sea Level
 $\frac{W}{q} = 11500 \frac{\#}{ft^3}$ $V_{st}/sec = 259$
 $\frac{W}{q} = 105000 \frac{\#}{ft^3}$ $C.G.R.A. = .280$
 $\frac{W}{q} = 80, \Delta = .175 \text{ ft.}$

$V_{st}/sec = 259$
 $C.G.R.A. = .280$

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

COEFFICIENTS OF EQUATIONS OF MOTION

RUNS # 58, 59, 60

	W'	B'	T'	X'	Y'	Z'	θ'	ϕ'	ψ'	d'	α'	β'	γ'	B'	B	B	B	$F.F.$		
Eq. 1	.04987	.04718	—	.01649	.02008	—	-.03039	-.2723	-.22.217	.001562	.03815	-.2998	.1633	.1815	.1828	.1411	.6931	.11.61		
2	-.01029	-.08550	—	-.053615	-.07776	—	.11.42	.12.64	.18.64	.3821	.8221	.938	-.5580	-.7659	-.6860	-.1.430	-.2.290	8.622		
3	.08166	.08125	—	.1570	.1710	—	-.2781	-.3861	-.24.36	-.01429	-.01429	-.34.94	-.22.25	1.029	1.836	1.402	5.347	9.236		
4	.002463	.005641	—	.008247	.008761	.03637	-.01519	-.02108	-.1.657	-.0007809	-.01907	-.1.237	.08166	.08395	.0779	.20.1	.3302	.5566		
5	—	-.001757	—	—	—	—	-.003202	-.006366	-.1835	-.1822	-.1610	-.1835	.3463	.8.823	—	-.02077	-.02932	-.03118	-.02244	-.163

ANTI-SYMMETRIC MOTION

	θ'	ϕ'	ψ'	d'	α'	β'	γ'	B'	B	B	$F.F.$						
Eq. 1	.90.42	1.90.9	—	1.491	2.311	—	-.1399	-.3.417	-.221.0	.14.91	.31.46	13.91	.39.79	.65.56	.266.7		
2	7.4453	6.8869	—	1.526	1.710	—	-.01429	-.34.94	-.22.25	.1.629	.1.816	1.402	5.347	9.232	12.68		
3	3.998	3.8850	—	.008247	.008761	.03637	-.0007809	-.01907	-.1.237	.08166	.08395	.0779	.20.1	.3302	.71.62		
4	.3998	-.4.527	—	—	-.003202	-.006366	.1835	.3463	.8.823	—	-.03077	-.07932	-.05118	-.02244	-.31.93		

PREPARED 9.A.M. 9-21-50
CHECKED _____
REVISED _____

Alt. = 844 Level
 $\frac{W}{84} = 11500 \text{ lb}$
 $\frac{W}{29} = 120000 \text{ lb}$
 $q_a = .80, q_c = .175 \text{ ft.}$

$V_{cr}/sec = 259$
 $C.G./84 = .280$

[CONFIDENTIAL] NO. EDR-C-905-204
W.C.S.

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

COEFFICIENTS OF EQUATIONS OF MOTION.

RUNS # 61, 62, 63

	W'	W	x'	y'	z'	g'	ϕ'	θ'	ψ'	α'	β'	γ'	\dot{x}'	\dot{y}'	\dot{z}'	$\dot{\phi}'$	$\dot{\theta}'$	$\dot{\psi}'$	\ddot{x}'	\ddot{y}'	\ddot{z}'
Eq. 1	.05553	.04718	--	.01669	.02008	--	.03039	--	.2723	-12.217	.001562	.03815	-2.998	.1633	.2655	.1888	.4421	.6934	.11.111	.11.111	
2	-.03039	-.08562	--	-.05615	-.07776	--	12.96	12.64	18.64	.3824	.8224	9.38	-.5560	-.2559	-.6860	-.1.490	-.2.294	8.622	1	1	
3	.08166	.09225	--	.2520	.1710	--	-.2781	-.2781	-.3861	-.26.36	-.01229	-.3194	-.22.25	1.629	1.836	2.402	5.347	9.232	12.69	1	
4	.001463	.0015621	--	.0082647	.0087651	.03637	-.10519	-.10519	-.02108	-.1.657	-.00072809	-.01907	-.1.237	.08166	.08355	.0779	.2012	.3302	.5565	1	
5	--	-.002797	--	--	-.009202	.006366	-.1885	-.1885	-.3822	-.4610	.1885	-.3463	-.8.823	--	-.02977	-.07232	-.05118	-.02244	-.04331	1	

ANTI-SYMMETRIC MOTION

	g'	ϕ'	θ'	ψ'	α'	β'	γ'	\dot{x}'	\dot{y}'	\dot{z}'	$\dot{\phi}'$	$\dot{\theta}'$	$\dot{\psi}'$	\ddot{x}'	\ddot{y}'	\ddot{z}'	$\ddot{\phi}'$	$\ddot{\theta}'$	$\ddot{\psi}'$
1	.93.07	190.9	--	1.691	2.311	--	-.1399	-.3.617	-.221.0	14.91	31.16	13.31	33.79	65.66	226.2	1	1	1	1
2	2.453	6.869	--	1.526	1.720	--	-.01229	-.34.94	-.22.25	1.629	1.836	2.402	5.347	9.232	12.69	1	1	1	1
3	3.998	.3880	--	.008247	.0087651	.03637	-.00072809	-.01907	-.3.237	.08166	.08355	.0779	.2012	.3302	.7162	1	1	1	1
4	--	-.4227	--	--	-.009202	.006366	-.1885	-.1885	-.3463	8.823	--	.09077	-.07232	-.05118	-.02244	-.31331	1	1	1

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[CONFIDENTIAL]

Mr. = Semilevel
 W₂₄ = 11500 #
 W₂₉ = 90000 #
 q = 140, a = 175 ft.

PREPARED
 CHECKED
 REVISED

Vt/sec = 344
 C.G./sec = .280
 W₂₄ = 140, a = .175 ft.

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
--	---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----

COEFFICIENTS OF EQUATIONS

TABLE II - D

OF MOTION

SINUSOIDAL

MOTION

RUNS # 64, 65, 66

	W ⁰	W ¹	W ²	Y ⁰	Y ¹	Y ²	θ ⁰	θ ¹	θ ²	ψ ⁰	ψ ¹	ψ ²	φ ⁰	φ ¹	φ ²	θ ⁰	θ ¹	θ ²	φ ⁰	φ ¹
Eq. 1	.0250	.0355	--	.0092	.0151	--	-.0174	-.2050	-.2217	-.0009	-.0287	-2.298	.0933	.1281	.1888	.1411	.6934	.5877		
2	-.0174	-.0640	--	-.0321	-.0586	--	5.608	9.520	18.64	.2185	.6192	9.380	-.3177	-.5766	-.6860	-.1490	-.2294	6.4392		
3	.0467	.0710	θ	.0872	.1288	--	-.1589	-.2307	-.2636	-.0082	-.2631	-22.25	.9309	1.382	1.402	5.347	9.232	9.5517		
4	.0026	.0042	--	.0017	.0066	.0008	-.0087	-.0159	-.1457	-.0004	-.0164	-1.237	.0467	.047	.0779	.2102	.3302	.4195		
5	--	-.0036	--	--	-.0069	.0036	.1077	.2878	.4610	.1077	.2603	5.260	--	-.0633	.0799	-.0512	-.0224	-.350 X		

ANTI-SYMMETRIC MOTION

	θ ⁰	θ ¹	θ ²	Y ⁰	Y ¹	Y ²	ψ ⁰	ψ ¹	ψ ²	φ ⁰	φ ¹	φ ²	θ ⁰	θ ¹	θ ²	φ ⁰	φ ¹	φ ²	θ ⁰	θ ¹
Eq. 1	50.13	143.7	--	35.50	1.240	θ	-.0729	-.7573	-.2210	8.570	23.69	11.91	39.79	65.66	170.71					
2	4.259	5.172	--	.0872	.1288	--	-.0082	-.2631	-.2225	.9299	1.382	1.402	5.347	9.232	9.5517					
3	2.285	.2922	--	.0017	.0066	.0008	-.0004	-.0164	-.1457	.0467	.047	.0779	.2102	.3302	.4195					
4	--	-.3401	--	--	-.0069	.0036	.1077	.2603	.5.260	--	-.0633	.0799	-.0512	-.0224	-.350 X					

CONFIDENTIAL

PREPARED BY: S. A. M. DATE: Sept-50
 CHECKED: _____ REVISED: _____

Alt. = Sea Level
 $\frac{V^2}{g} = 11500 \text{ ft}$
 $\frac{V^3}{g^2} = 105000 \text{ ft}^2$
 $\frac{V^4}{g^3} = 10500 \text{ ft}^3$
 $Q = 160, a = .175 \text{ ft.}$

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 MODEL 1

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

COEFFICIENTS OF EQUATIONS OF MOTION
SYMMETRIC MOTION

RUNS #67, 68, 69

	θ'	θ	θ''	θ'''	θ^1	θ^2	θ^3	θ^4	θ^5	θ^6	θ^7	θ^8	θ^9	θ^10	θ^11	θ^12	θ^13	θ^14	θ^15	θ^16
Eq. 1	.02838	.03552	--	.0094223	.01512	--	-.01737	-.02050	-.02217	-.02872	-.02998	.09331	.1381	.1888	.4411	.6924	.8587	X		
2	-.01737	-.06401	--	-.03209	-.08855	--	6.526	9.520	18.64	.2185	.6132	9.380	-.3177	-.5766	-.6860	-.1490	-2.294	6.458	X	
3	.01666	.07036	--	.08720	.1288	--	-.1589	-.2907	-.24636	-.008166	-.2631	-.22.25	.9109	1.382	1.402	5.342	9.232	9.556	X	
4	.002550	.0016247	--	.002713	.0085395	.002079	-.0056580	-.015872	-.01457	-.0084462	-.00516	-.1.237	.06636	.06721	.0779	.2021	.3392	.4391	X	
5	--	-.0031612	--	--	-.008328	.0036537	.0077	.2578	.1610	.1077	.2608	.5.260	--	-.06836	-.07992	-.05118	-.02244	-.3456	X	

ANTI-SYMMETRIC MOTION

	θ'	θ	θ''	θ'''	θ^1	θ^2	θ^3	θ^4	θ^5	θ^6	θ^7	θ^8	θ^9	θ^10	θ^11	θ^12	θ^13	θ^14	θ^15	θ^16
Eq. 1	51.67	143.7	--	.5520	1.740	--	-.07394	-.2.573	-.221.0	8.520	23.69	13.91	39.79	65.66	120.71					
2	4.259	5.172	θ^-	.08720	.1288	--	-.008166	-.2.631	-.22.25	.9309	1.282	1.402	5.342	9.232	9.556	X				
3	.2285	.2922	--	.004713	.008596	.002079	-.00004462	-.01436	-.01237	.06636	.06721	.0779	.2021	.3392	.4391					
4	--	-.3408	--	--	-.0063928	.0036537	.0077	.2578	.1610	.1077	.2608	.5.260	--	-.06836	-.07992	-.05118	-.02244	-.3456	X	

PREPARED 6-11-50
CHECKED _____
REVISED _____

Alt. = Sea Level
 ■ 84 = 11500 ft
 ■ 29 = 120000 ft
 q = 240, a =

45
ED-C-905-204

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PREPARED A. M. 9-2-50
CHECKED _____
REVISED _____

Alt. • Sea Level
 \times x_{84} • 11,500 ft.
 x_{29} • 10,500 ft.
Q • 200, a • .175 ft.

$V_{\text{sec}} = 410$
 $G/G_{84} = .280$

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REF ID: A4 NO. EDR-C905-104

		COEFFICIENTS OF EQUATIONS OF MOTION																								
		SYMMETRIC MOTION																								
		α'	β'	γ'	θ'	ϕ'	ψ'	α''	β''	γ''	θ''	ϕ''	ψ''	α'''	β'''	γ'''	θ'''	ϕ'''	ψ'''	$\alpha^{(4)}$	$\beta^{(4)}$	$\gamma^{(4)}$	$\theta^{(4)}$	$\phi^{(4)}$	$\psi^{(4)}$	
Eq. 1	.019877	.02980	—	.006596	.01269	—	-.01216	-.1720	-.12.217	-.000624	-.02410	2.998	.065932	.1159	.1688	.4411	.6934	.7.208 X	—	—	—	—	—	—		
2	—	.01216	-.01532	—	-.02216	-.01912	—	-.568	7.988	18.64	.1530	.5195	9.38	—	-.2224	-.4838	-.6860	-.1.29	.2.294	5.442 X	—	—	—	—	—	
3	—	.02266	.05756	—	—	.06104	.1080	—	-.1112	-.2429	-.26.36	—	.005716	-.2207	-.22.25	.6516	1.1180	1.402	5.362	9.232	6.016 X	—	—	—	—	—
4	—	.001785	.003563	—	—	.003299	.005524	.01455	-.006076	-.01332	-.2.457	—	.0003324	-.01205	-.1.237	.5266	.05269	.0779	.2001	.3202	.3.516 X	—	—	—	—	—
5	—	—	—	—	—	.002010	.005813	.002546	.01540	.2445	.4610	.07540	.2188	.3.835	—	—	-.05734	-.07392	-.05118	-.02244	-.2933 X	—	—	—	—	—
ANTI-SYMMETRIC MOTION																										
Eq. 1	36.17	120.6	—	5264	3.60	—	-.05526	-2.159	-.221.0	5.266	12.88	13.91	39.79	65.66	113.2 X	—	—	—	—	—	—	—	—	—	—	
2	2.981	4.339	—	—	.06104	—	—	-.005716	-.2207	-.22.25	.6516	1.1160	1.402	5.347	9.292	8.010 X	—	—	—	—	—	—	—	—	—	—
3	1.1599	.2431	—	—	.032529	.055524	.01455	-.0003324	-.01205	-.1.237	.5266	.05269	.0779	.2001	.3202	.3.516 X	—	—	—	—	—	—	—	—	—	—
4	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

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PREPARED
CHECKED
REVISIED

AB. = 20000 ft.
B₂₄ = 14500 ft.
B₂₉ = 90000 ft.
q²⁹ = 80, **a** = .175 ft.

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E.O. 11

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF EQUATIONS OF MOTION. SYMMETRIC MOTION.																					
RADIUS \Rightarrow B2, B3, B4																					
θ^1																					
B₁, 1	.04682	.0316	--	.0210	.0112	--	--	-.0384	-.1995	-.32,217	-.0020	-.02	-.2,998	.2,068	.1362	.1888	.1411	.6921	.10,203	■	
2	-.0384	-.0622	--	-.0212	-.0520	--	--	.03	.9,27	.18,64	.4,310	.692	.9,38	-.70,15	-.696	-.561	-.1,190	-.2,294	■	15	
3	.1022	.06896	--	.1220	.1234	--	--	-.3515	-.2325	-.24,36	-.0283	-.2557	-.22,25	2,082	1,342	1,012	5,317	9,292	31,321	■	
4	.0057	.0042	--	.0104	.0064	.0261	-.0192	-.0155	-.1,157	-.0110	-.0140	-.1,217	-.0132	.0828	.0729	.2040	.3302	.1363	■	100	
5	--	-.0035	--	--	-.0067	.0063	.2235	.280	.458	.2135	.2540	.8,529	--	-.0466	-.0800	-.2522	-.0222	-.4141	■	100	
ANTI-SYMMETRIC MOTION																					
θ^1																					
B₂, 1	106.5	1329.7	--	1,885	1,635	--	--	-1,765	-2,505	-221,0	18,684	23,05	13,21	39,78	65,66	225,01	■	11	11		
2	9.63	5.02	--	1,391	1,256	--	--	-.0121	-.2,357	-.22,25	2,082	1,342	1,012	5,317	9,292	12,581	■	15	15		
3	.505	.2840	--	.0104	.0064	.0261	-.0192	-.0155	-.1,157	-.0110	-.0140	-.1,217	-.0132	.0828	.0729	.2040	.3302	.1363	■	100	
4	--	-.3325	--	--	-.067	.063	.2135	.2540	.8,529	--	-.0466	-.0800	-.2522	-.0222	-.4141	■	100	100			

PREPARED
CHECKED
REVIEWED

Alt. = 20000 Ft.
Vft/sec = 354
C.G. 84 = .280
N 29 = 80.8 = 175 ft.

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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF EQUATIONS OF MOTION RUNS # 66, 84, 87																					
SYMMETRIC MOTION																					
	θ'	θ''	φ'	φ''	y'	y''	θ^*	$\theta^{\prime\prime}$	φ^*	$\varphi^{\prime\prime}$	ψ^*	$\psi^{\prime\prime}$	$\theta^{\prime\prime\prime}$	$\theta^{\prime\prime\prime}$	$\varphi^{\prime\prime\prime}$	$\psi^{\prime\prime\prime}$	$\theta^{\prime\prime\prime}$	$\theta^{\prime\prime\prime}$	$\varphi^{\prime\prime\prime}$	$\psi^{\prime\prime\prime}$	
Eq.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
1	.0520	.0346	--	.0210	.0147	--	-.0384	-.1995	-.12.217	-.0020	-.0280	-.2.998	.2.068	.13.42	.1838	.4.411	.6.924	-.10.20X			
2	-.0384	-.0622	--	-.0512	-.0510	--	11.49	9.27	18.64	.4.310	.6.02	.9.38	-.70.5	-.5.61	-.6.86	-.14.20	-.2.22L	-.7.73 X			
3	.0332	.06896	--	.1930	.1256	--	-.3515	-.2825	-.24.36	-.0191	-.2557	-.22.65	2.082	1.362	1.602	5.327	9.532	11.32 X			
4	.0057	.00622	--	.0102	.0064	.0163	-.0192	-.0155	-.01457	-.0020	-.0040	-.1.237	.1.032	.0.628	.0.779	.2.640	.3.02	.4.96 X			
5	--	-.0035	--	--	-.0067	.0063	.2135	.280	.458	.2135	.2.940	.8.829	--	--	-.0666	-.0500	-.5.512	-.0.221	-.4.44 X		
ANTI-SYMMETRIC MOTION																					
	θ'	θ''	φ'	φ''	y'	y''	θ^*	$\theta^{\prime\prime}$	φ^*	$\varphi^{\prime\prime}$	ψ^*	$\psi^{\prime\prime}$	$\theta^{\prime\prime\prime}$	$\theta^{\prime\prime\prime}$	$\varphi^{\prime\prime\prime}$	$\psi^{\prime\prime\prime}$	$\theta^{\prime\prime\prime}$	$\theta^{\prime\prime\prime}$	$\varphi^{\prime\prime\prime}$	$\psi^{\prime\prime\prime}$	
Eq.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
1	109.19	139.7	--	1.885	1.675	--	-.1765	-.2.505	-.221.0	18.88	23.05	13.91	39.78	65.66	225.0X						
2	9.43	5.02	--	1.192	.1256	--	-.0181	-.2.537	-.22.25	2.082	1.362	1.602	5.327	9.532	12.52 X						
3	.505	.280	--	.212	.0064	.0363	-.0110	-.0170	-.01.237	.1.032	.0.628	.0.779	.2.640	.3.02	.4.96 X						
4	--	-.3315	--	--	-.0067	.0063	.2135	.250	.8.829	--	-.0666	-.0500	-.0.221	-.3.16 X							

CONFIDENTIAL

PREPARED
CHECKED
REVISED

Alt. = 20000 ft.
W₈₄ = 145000 lb.
W₂₉ = 90000 lb.
q = 120 lb = .175 ft.



PAGE 52
REF ID: A74031 W.C. EDR-0905-304

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE III COEFFICIENTS OF MOTION RUNS 91, 92, 93																					
SYMMETRIC MOTION																					
$K = 0$ $K = 1.5$ $K = 3.0$																					
W	W'	W	Y'	Y	Y"	θ'	θ	θ"	ε'	ε	ε"	β'	β	β"	β'	β	β"	β'	β	β"	
Eq. 1	.0308	.0282	--	.0140	.0120	--	--	--	.0036	-.1625	-.22.237	-.00013	-.0028	-.2.298	.1378	.1095	.1813	.4411	.6924	-.9.31 X	
2	-.0856	-.0507	--	-.0674	-.0454	--	--	--	.6.61	7.55	28.66	2.928	.621	9.38	-.1.70	-.457	-.686	-.1.690	-.2.296	6.30 X	
3	.0688	.05624	--	.1327	.1021	--	--	--	-.2345	-.230	-.26.36	-.0211	-.2185	-.2.25	1.388	1.095	1.402	5.347	9.292	9.23 X	
4	.0037	.0034	--	.0069	.0052	--	--	--	.0126	-.0128	-.0126	-.1.657	-.0007	-.0.81	-.1.237	.0689	.0512	.0779	.2060	.3302	.404 X
5	--	-.3849	--	--	-.0055	.0012	.2.25	.228	.658	.2.25	.2.25	.2.25	.6.019	--	-.0543	-.0800	-.0512	-.0221	-.338 X		
ANTI-SYMMETRIC MOTION																					
$K = 0$ $K = 1.5$ $K = 3.0$																					
g	g'	g	x'	x	x"	ε'	ε	ε"	β'	β	β"	β'	β	β"	P	P'	P	P'	P	P'	
Eq. 1	71.0	113.8	--	1.257	1.280	--	--	--	-.1178	-.2.020	-.22.20	12.58	18.77	13.91	39.78	65.66	183.1 X				
2	6.29	4.09	--	.1328	.1021	--	--	--	-.0120	-.2185	-.22.25	1.388	1.085	1.402	5.347	9.292	10.24 X				
3	.3365	.2315	--	.0069	.0052	--	--	--	.0212	-.0007	-.0014	-.1.237	.0688	.0512	.0779	.2040	.3302	.5082 X			
4	--	-.270	--	--	-.0005	.0012	.2.25	.225	.6.019	--	--	-.0543	-.0800	-.0512	-.0221	-.252 X					

PREPARED
CHECKED
REVISED

Alt. = 20000 ft. $V = 424 \text{ ft/sec}$.
 ■ 84 = 14500 ft. $\alpha = .280$
 ■ 84 = 105000 $\beta = .280$
 ■ 29 = 120 a = .175 ft.

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REF ID: A62646 EDR-0905-104

CONFIDENTIAL

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION RUNS #94, 95, 96																					
SYMMETRIC MOTION																					
$K = 0$ $K = 1.5$ $K = 3.0$																					
	β^*	β'	β''	γ^*	γ'	γ''	α^*	α'	α''	β^*	β'	β''	β^*	β'	β''	β^*	β'	β''	β^*	β'	
Eq. 1	.0347	.0232	—	.0120	.0120	—	-.0256	-.1625	-.12.217	-.2013	-.0828	-.2.38	.3378	.1095	.1388	.4611	.6934	.8311			
2	-.0256	-.0507	—	-.0466	—	—	7.65	77.55	18.64	22.8	.491	9.38	-.470	-.457	-.436	-.430	-.429	-.428	6.30 X		
3	.0688	.05624	—	.1327	.1021	—	-.2345	-.230	-.23.36	-.0121	-.2185	-.22.25	1.388	1.095	1.402	5.347	9.222	9.223 X			
4	.0037	.0034	—	.0069	.0052	—	-.0126	-.0128	-.0126	-.0126	-.0007	-.0114	-.2.237	.0689	.0512	.0779	.2040	.3302	.404 X		
5	—	-.0029	—	—	—	—	-.0005	.0042	.1425	.228	.4658	.225	.2067	.6.069	—	-.0512	-.0512	-.338X			
ASYMMETRIC MOTION																					
	β^*	β'	β''	γ^*	γ'	γ''	α^*	α'	α''	β^*	β'	β''	β^*	β'	β''	β^*	β'	β''	β^*	β'	
Eq. 1	.7279	113.8	—	1.257	1.380	—	-.11.8	-.2.040	-.1.0	12.58	16.77	13.91	39.78	65.66	183.1 X						
2	6.29	4.09	—	.1328	.1021	—	-.0120	-.0120	-.0120	-.2185	-.22.25	1.388	1.095	1.402	5.347	9.222	10.24 X				
3	.3365	.2315	—	.0069	.0052	—	.0242	-.0007	-.0014	-.00237	.0683	.0512	.0779	.2040	.3302	.5782 X					
4	—	-.270	—	—	—	—	-.0055	.0042	.1425	.2067	.6.049	—	-.0513	-.0800	-.0512	-.0221	-.2.57 X				

CONFIDENTIAL

PREPARED _____
CHECKED _____
REVISED _____


 Alt = 20000 ft. V = .634 ft/sec
 W₈₄ = 14500 lb C. G. = .280
 W₂₉ = 120000
 q₂₉ = 120 a. = .175 ft.

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CONFIDENTIAL
REF-C905-104

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION. AUGUST 97, 98, 99																					
SYMMETRIC MOTION																					
θ^1 θ^2 θ^3 θ^4 θ^5 θ^6 θ^7 θ^8 θ^9 θ^10 θ^11 θ^12 θ^13 θ^14 θ^15 θ^16 θ^17 θ^18 θ^19 θ^20 θ^21																					
Eq. 1	.0386	.0282	—	.0140	.0020	—	-.0056	-.1625	-.32.237	-.2013	-.0228	-.2.298	.1378	.1095	.1883	.1111	.6.924	-.3.311			
2	-.0256	-.0507	—	-.0474	-.0064	—	8.59	7.55	18.64	.2832	.491	9.38	-.670	-.457	-.686	-.1.490	-.2.294	6.30			
3	.0688	.05624	—	.1327	.1021	—	-.2365	-.230	-.24.36	-.0211	-.2185	-.22.25	1.388	1.095	1.402	5.347	9.280	9.23			
4	.0037	.0024	—	.0069	.0052	.0242	.0128	-.0126	-.2.457	-.0007	-.0114	-.1.237	.0689	.0512	.0779	.2040	.3302	.041			
5	—	-.0029	—	—	-.0055	.0042	.0125	.228	.458	.2025	.2067	6.009	—	-.563	-.0800	-.0512	-.2.22	-.338			
ANTI-SYMMETRIC MOTION																					
ϕ^1 ϕ^2 ϕ^3 ϕ^4 ϕ^5 ϕ^6 ϕ^7 ϕ^8 ϕ^9 ϕ^10 ϕ^11 ϕ^12 ϕ^13 ϕ^14 ϕ^15 ϕ^16 ϕ^17 ϕ^18 ϕ^19 ϕ^20 ϕ^21																					
Eq. 1	74.56	113.8	—	1.257	1.330	—	-.11.78	-.2.000	-.321.0	12.58	18.77	13.91	39.78	65.66	183.11						
2	6.29	4.09	—	.1328	.1021	—	-.0220	-.2185	-.32.235	1.383	1.095	1.622	5.347	9.280	10.26						
3	.3365	.2115	—	.0069	.0052	.0242	-.0007	-.0024	-.2.237	.0688	.0512	.0779	.2040	.3302	.5752						
4	—	-.270	—	—	-.0055	.0042	.0125	.2067	.6.009	—	-.0513	.0800	-.0512	-.2.21	-.2.57						

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 CHECKED _____
 REVISED _____

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 MODEL

Altitude = 20,000 ft. V = 501 ft/sec.

W₁₅₄ = 14,500 lbs.

W₂₉ = 90,000 lbs.

a = 160 b = .175 ft. g_{bar} = .280

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
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COEFFICIENTS OF EQUATIONS OF MOTION
 RUNS #100, 101, 102

	ω'	ω''	ψ'	ψ''	θ'	θ''	α'	α''	β'	β''	γ'	γ''	δ'	δ''	ϵ'	ϵ''	ζ'	ζ''	ξ'	ξ''
Eq. 1	.02371	.0245	-	.0105	.0104	-	-.0192	-.1111	.12.237	-.0010	-.01972	-.2.993	.1033	.0950	.1838	.4411	.634	.7.211		
2	-.0192	-.0440	-	-.0355	-.0403	-	..4.96	6.55	18.64	.2168	.426	9.38	-.3520	-.3965	-.686	-.1490	-.2.294	5.472		
3	.05156	.05872	-	.0995	.0857	-	-.1723	-.1993	-.24.36	-.0090	-.1.306	-.22.25	1.040	.950	1.402	5.347	9.522	8.011		
4	.0028	.0030	-	.005221	.0015	.0182	-	.0096	-.0110	-.1.457	-.0006	-.0099	1.1.237	.0517	.0444	.0779	.2040	.3702	.3.511	
5	—	-.0025	-	—	—	-.0047	.0032	.1028	.1980	.4.58	.1048	.1797	4.669	—	—	-.0471	-.0700	-.0512	-.0221	-.2.931

ANTI-SYMMETRIC MOTION

	ϕ'	ϕ''	ψ'	ψ''	α'	α''	β'	β''	γ'	γ''	δ'	δ''	ϵ'	ϵ''	ζ'	ζ''	ξ'	ξ''	
Eq. 1	53.25	98.75	-	36.25	1.198	-	-.0822	-.22.20	9.44	16.32	13.91	29.78	65.66	159.0					
2	4.72	3.55	-	.0995	.0857	-	-.0090	-.1895	-.22.25	1.042	.950	1.402	5.347	9.522	8.011				
3	.02325	.0210	-	.0052	.0015	.0182	-.0006	-.0099	1.237	.0515	.0444	.0779	.2040	.3702	.3.509				
4	—	.2315	-	—	—	-.0047	.0032	.1028	.1797	4.669	—	-.0471	-.0800	-.0512	-.0221	-.2.224	I		

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PREPARED _____
 CHECKED _____
 REVISED _____
 Altitude = 20,000 ft. V = 501 ft/sec
 W₂₄ = 10,500 lbs. a = .175 ft
 W₂₉ = 10,500 lbs. CG₂₄ = .280
 q = 160

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF EQUATIONS OF MOTION.																					
RUNS # 103, 134, 105																					
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
SYMMETRIC MOTION																					
	ω'	ω	ω_1	ω_2	ω_3	ω_4	ω_5	ω_6	ω_7	ω_8	ω_9	ω_{10}	ω_{11}	ω_{12}	ω_{13}	ω_{14}	ω_{15}	ω_{16}	ω_{17}	ω_{18}	
Eq. 1	.0260	.0245	-	.0105	.0104	-	-	.0192	.-1.01	-12.02	.0010	.-01972	2.996	.0133	.0950	.1833	.0411	.0931	.7.211		
2	.-0192	.-0.0440	-	.-0.0355	.-0.0403	-	-	.5.74	6.55	18.64	.0268	.6.23	2.03	.-3.20	.-5.965	.-1.490	.-2.254	.5.47	.01		
3	.0316	.04872	-	.0595	.0687	-	-	.-1758	.-1.998	.-24.36	.-0.0090	.-1.896	.-22.25	.1.040	.950	.1.402	.5.347	.2.29	.0.01		
4	.0028	.0030	-	.0052	.0045	.0182	-	.0096	.-0.0110	.-1.457	.-0.0066	.-0.099	.-1.0237	.0517	.0144	.0779	.2040	.3932	.2511		
5	-	.-0.0025	-	-	.-0.0047	.0032	.1043	.1980	.450	.1048	.1797	4.669	-	.-0.0471	.0.000	.-0.532	.-0.221	.-0.231			
ANTI-SYMMETRIC MOTION																					
	Φ'	Φ	Ψ	Ψ_1	Ψ_2	Ψ_3	Ψ_4	Ψ_5	Ψ_6	Ψ_7	Ψ_8	Ψ_9	Ψ_{10}	Ψ_{11}	Ψ_{12}	Ψ_{13}	Ψ_{14}	Ψ_{15}	Ψ_{16}	Ψ_{17}	
Eq. 1	54.59	98.75	-	.9425	1.196	-	-	.0252	.-1.770	.-221.0	9.64	16.30	13.1	39.78	65.66	159.0					
2	4.72	3.55	-	.00995	.0897	-	-	.0090	.-1.295	.-22.25	.1042	.950	.1.402	.5.347	.9.29	.2.91					
3	.2325	.2010	-	.0052	.0045	.0132	-	.0306	.-0.092	.-1.337	.0515	.6.664	.0779	.5046	.3900	.5000					
4	-	.-2.345	-	-	.-0.0147	.0032	.1048	.1797	4.669	-	.-0.072	.-0.000	.-0.532	.-0.221	.-0.231						

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PREPARED _____
 CHECKED _____
 REVISED _____

Altitude = 20,000 ft. V = 501 ft/sec.
 W₂₄ = 14,500 lbs. e = .175 ft.
 W₂₉ = 120,000 lbs. CG₁₄ = .280
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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
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TABLE II-D
 COEFFICIENTS OF EQUATIONS OF MOTION.
 DOWNS # 106, 107, 108

SIMMETRIC MOTION

	ω_{11}	ω_{12}	ω_{13}	ω_{14}	ω_{15}	ω_{16}	ω_{17}	ω_{18}	ω_{19}	ω_{110}	ω_{111}	ω_{112}	ω_{113}	ω_{114}	ω_{115}	ω_{116}	ω_{117}	ω_{118}	ω_{119}	ω_{110}	
Eq. 1	.0289	.0245	-	.0105	.0104	-	-.0192	-.2411	-.12.217	.0010	-.21972	-2.998	.2033	.0950	.1888	.4411	.6934	-7.211			
2	-.0122	-.0440	-	-.0355	-.0403	-	6.52	6.55	16.64	.2168	.426	9.38	.2520	-.3965	-.686	1.490	-2.294	5.474			
3	.0516	.04572	-	.0995	.0827	-	-.1758	-.1998	-.24.36	-.0630	-.1306	20.25	1.040	.050	1.402	5.347	9.392	.0.011			
4	.0028	.0030	-	.0052	.0145	.0182	-.0996	-.0110	-.1.457	-.0006	-.0999	-.1.237	.0517	.0114	.0114	.0779	.2010	.3302	.0.311		
5	-	-.0025	-	-.0047	.0032	.1048	.1930	.458	.1048	.1797	4.669	-	-.0171	-.0300	-.0112	-.0221	-.293				

ANTI-SYMMETRIC MOTION

	α_{11}	α_{12}	α_{13}	α_{14}	α_{15}	α_{16}	α_{17}	α_{18}	α_{19}	α_{110}	α_{111}	α_{112}	α_{113}	α_{114}	α_{115}	α_{116}	α_{117}	α_{118}	α_{119}	α_{110}	
Eq. 1	55.92	98.75	-	.9425	1.190	-	-.0152	-.17.0	221.0	9.44	16.30	13.91	39.78	65.66	159.0X						
2	4.72	3.55	-	.0995	.037	-	-.0090	-.1795	22.25	1.02	.930	1.402	5.747	9.292	6.90X						
3	.2525	.2010	-	.0052	.0045	.0182	-.0066	-.0099	1.237	.0115	.0644	.0779	.0340	.0302	.009X						
4	-	-.2345	-	-.0047	.0022	.1048	.1797	4.669	--	-.0171	-.0300	-.0112	-.0221	-.293							

CONFIDENTIAL

Altitude =	20,000 ft.	q =	80
in S4	= 13,000 lbs.	g =	.354 ft./sec
W29	= 90,000 lbs.	a =	.175 ft./sec
		CCG =	.280

PREPARED
CHECKED
REVISED

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF EQUATIONS OF MOTION																					
RUNS # 109, 110, 111																					
SYMMETRIC MOTION																					
α_{xx}	ω_x	ω_y	γ_x	γ_y	β_x	β_y	θ_x	θ_y	α_x	α_y	β_x	β_y	γ_x	γ_y	α_x	α_y	β_x	β_y	γ_x	γ_y	θ_x
.0450	.0346	-	.0188	.0127	-	-	.0244	.1995	12.217	.0118	.0280	2.998	.1852	.1362	.1888	.4411	.6034	-10.201			
-0.344	.0622	-	-	.0638	.0570	-	9.88	.9.27	18.64	.2000	.302	9.38	-.621	-.561	-.636	-1.630	-2.024	5.732			
.0926	.06896	-	-	.1787	.1254	-	-	.315	.2225	-24.36	.0162	-.2557	22.25	1.867	1.342	1.402	5.367	9.292	11.321		
.0051	.0042	-	-	.00936	.0061	.0363	-	.0172	-.0155	-1.457	.0009	-.01040	-1.237	.0925	.0626	.0779	.2040	.3302	.4961		
-	-.0035	-	-	-	-.0057	.0063	.1905	.200	.458	.1916	.2540	8.829	-	-.0666	-.0300	-.0512	-.0221	-.1141			
ASYMMETRIC MOTION																					
α_{yy}	ϕ	ψ	γ_x	γ_y	β_x	β_y	α_x	α_y	β_x	β_y	γ_x	γ_y	α_x	α_y	β_x	β_y	γ_x	γ_y	ϕ	ψ	
97.26	139.7	-	1.690	1.695	-	-	-1.983	-2.905	-221.0	16.92	23.05	13.91	39.73	65.66	225.01						
8.66	5.02	-	-	.1777	.1254	--	-	.0162	-.2557	-22.25	1.867	1.342	1.402	5.367	9.292	12.083					
.43	.2640	-	.00926	.004	.0363	-	.0009	-.01040	-1.237	.0925	.0626	.0779	.2040	.3302	.4961						
-	-2.315	-	--	-.0067	.0063	.1906	.2540	8.829	--	-.0666	-.0300	-.0512	-.0221	-.1141							

PREPARED
CHECKED
REVIEWED

Altitude = 20,000 ft. V = 354 ft./sec.
W₂₄ = 13,000# a = .175 ft.
W₂₉ = 120,000# CG₂₄ = .280

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REF ID: EDR-C-905-105

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
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TABLE II - D
COEFFICIENTS OF EQUATIONS OF MOTION
RUNS # 115, 116, 117

SYMMETRIC MOTION																			
	ω	ω'	ω''	φ	φ'	φ''	θ	θ'	θ''	α	α'	α''	β	β'	β''	γ	γ'	γ''	F. F.
1	.0567	.0346	-	.0188	.0147	-	.0344	-.1995	-.12.217	.0018	.0280	-2.998	.1842	.1852	.1888	.4411	.6924	-.10.201	
2	-.0344	.0622	-	.0638	-.0570	-	-.13.00	.9.27	18.64	.3890	.602	9.38	-.631	-.561	-.596	-.1.490	.7.294	.7.732	
3	.0926	.06896	-	.2787	.1254	-	.315	.2825	-.26.36	-.0162	.2557	-.22.25	1.867	1.312	1.402	.5.947	9.292	11.322	
4	.0021	.0042	-	.00936	.0064	.0363	.0172	.0155	-.2.457	.0009	-.0140	-.2.237	.0925	.0628	.0779	.2.40	.3302	.4962	
5	-	.0035	-	-	-.0067	.0063	.1915	.280	.458	.1916	.2540	8.829	-	-.0666	-.0890	-.0512	-.0271	-.1144	

ANTI-SYMMETRICAL

ANTI-SYMMETRICAL																			
	δ	δ'	δ''	φ	φ'	φ''	α	α'	α''	β	β'	β''	γ	γ'	γ''	β	β'	β''	F. F.
1	102.6	139.2	-	1.680	1.695	-	-.1583	-2.505	-.221.0	16.92	23.05	13.91	32.78	65.66	225.0	1	1	1	
2	84.6	5.02	-	.1787	.1224	--	-.0162	-.2557	-.22.25	1.067	1.302	1.402	5.347	9.992	12.55	2	2	2	
3	-.453	.2540	-	.00936	.0064	.0363	-.0009	-.0363	-.0140	-.1.236	.0925	.0628	.0779	.2040	.3302	.7090	3	3	3
4	-	.3315	-	-	-.0067	.0063	.1916	.2540	8.829	-	-.0666	-.0890	-.0512	-.0271	-.1144	316	4	4	

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PREPARED 61
 CHECKED 61
 REVISED 61
 Alt. = 20,000 ft. $V = 434 \text{ ft/sec}$
 FB₄ = 13,000 # $a = 175 \text{ ft.}$
 FB₉ = 90,000 # $c_{684} = .280$
 q = 2.0

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

TABLE II-D
COEFFICIENTS OF MOTION
RUNS # 116, 119, 120

	SYNTHETIC MOTION										ARTIFICIAL MOTION										
	ϕ''	ϕ'	ψ''	ψ'	y''	y'	θ''	θ'	α''	α'	β''	β'	γ''	γ'	δ''	δ'	ϵ''	ϵ'	ζ''	ζ'	
Bl. 1	.0300	.0282	.0125	.0120	-.0029	-.0025	-.1625	-.12.217	-.0012	-.0228	-.2.998	.1234	.1095	.1888	.4411	.6934	-.3.31				
2	-.0229	-.0507	.0425	.0464	6.58	7.55	18.64	.2552	.491	.2.28	.421	-.457	-.696	-.1430	-.457	-.2.24	6.30				
3	.0617	.05624	.1190	.1001	-.2310	-.2436	-.2108	-.2185	-.22.25	-.2.244	1.095	1.422	5.347	9.292	9.233						
4	.0034	.0034	.00622	.00622	-.2462	-.0115	-.0126	-.1.657	-.0006	-.0114	-.1.237	.0617	.0512	.0779	.2040	.3.302	.4.04				
5	-.0029		.00162	.00162	.1.73	.228	.458	.4278	.2.067	.6.049	-.0543	-.0800	-.0512	-.0221	-.3.381						

	SYNTHETIC MOTION										ARTIFICIAL MOTION										
	ϕ''	ϕ'	ψ''	ψ'	y''	y'	θ''	θ'	α''	α'	β''	β'	γ''	γ'	δ''	δ'	ϵ''	ϵ'	ζ''	ζ'	
Bl. 1	113.8	1.127	1.130	-.1056	-.2.040	-.221.0	11.28	18.77	13.91	39.78	65.66	183.1X									
2	5.64	4.09	.1190	.1021	-.0108	-.2185	-.22.25	1.244	1.095	1.402	5.347	9.292	10.23X								
3	.302	.2315	.00623	.00622	-.0042	-.0006	-.0114	-.1.237	.0617	.0512	.0779	.2040	.3.302	.5782X							
4		-.270		-.0055	.0042	.1278	.2067	.6.049	-.0543	-.0800	-.0512	-.0221	-.3.371								

PREPARED
CHECKED
REVIEWED

11t. = 20,000 ft. **V = .34 ft./sec.**
WB4 = 13,000 # **A = .175 ft.**
R29 = 105,000 # **c884 = .280**
q = 120

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[CONFIDENTIAL]
 PROJ. NO. 0905-104

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
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TABLE III-D
COEFFICIENTS OF VARIATIONS OF MOTION

SIMPLIFIED MOTION

	ω	ω	θ																
Eq. 1	.0339	.0282	.0125	.0120	-.0229	-.1625	-.1217	-.0012	-.0228	-.0228	-.0234	.1095	.1888	.4411	.6924	.8311			
2	-.0229	-.0507	-.0425	-.0464	7.62	7.55	18.64	25.92	6.91	9.38	-.421	-1.457	-.686	-1.490	-2.294	6.301			
3	.0617	.05624	.1190	.1321	-.210	-.230	-.24.36	-.0108	.2185	-.22.25	1.244	1.095	1.402	5.347	9.292	9.211			
4	.0034	.0034	.00623	.0052	.0242	-.0115	-.0126	-.457	-.0006	.0114	-.237	.0617	.0512	.9779	.2040	.3302	.4041		
5	-.0029		-.0055	.0042	.1278	.228	.458	.1278	.2067	.6.09		-.0513	-.080	-.0512	-.0221	-.3381			

ANTI-SYMMETRIC MOTION

	θ																		
Eq. 1	66.6	113.8	1.127	1.390	-.1056	-.040	-.221.0	11.28	18.77	13.91	39.78	65.66	183.11						
2	5.64	4.09	.1190	.1321	-.0108	-.2185	-.22.25	1.244	1.095	1.402	5.347	9.292	10.21						
3	.302	.2315	.20623	.0052	.0242	-.0006	-.0114	-.1.237	.0617	.0512	.0779	.2040	.3302	.57821					
4	-.270		-.0055	.0042	.1278	.2067	.6.09		-.0513	-.080	-.0512	-.0221	-.2571						

[CONFIDENTIAL]

Alt. = 20,000 ft. V = 434 ft/sec
 W84 = 13,000 # a = .175 ft.
 W29 = 120,000 # og84 = .280
 q = 120

PREPARED _____
 CHECKED _____
 REVISED _____
 CONFIDENTIAL REPORT NO. EUR-2905-104
 Dated _____

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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II EQUATIONS OF MOTION																					
COEFFICIENTS OF MOTION																					
RUNS 124, 125, 126																					
SYMMETRIC MOTION																					
W ₁ W ₂ W ₃ W ₄ W ₅ W ₆ W ₇ W ₈ W ₉ W ₁₀ W ₁₁ W ₁₂ W ₁₃ W ₁₄ W ₁₅ W ₁₆ W ₁₇ W ₁₈ W ₁₉ W ₂₀ W ₂₁																					
Eq. 1																					
1	.0378	.0282	.0125	.0120																	
2	-.0229	-.0507	-.0425	-.0464																	
3	.0617	.05624	.1190	.1021																	
4	.0034	.0034	.00623	.0032																	
5	-.0029		-.0035	.0242																	
ANTI-SYMMETRIC MOTION																					
Φ ₁ Φ ₂ Φ ₃ Φ ₄ Φ ₅ Φ ₆ Φ ₇ Φ ₈ Φ ₉ Φ ₁₀ Φ ₁₁ Φ ₁₂ Φ ₁₃ Φ ₁₄ Φ ₁₅ Φ ₁₆ Φ ₁₇ Φ ₁₈ Φ ₁₉ Φ ₂₀ Φ ₂₁																					
Eq. 1																					
1	68.36	113.8	1.127	1.380																	
2	5.64	4.09	.1190	.1021																	
3	.302	.2315	.00623	.0052																	
4	-.270		-.0055	.0042																	

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Alt. = 20,000 ft. V = 501 ft/sec.
 NBG = 13,000 # a = .175 ft.
 R29 = 90,000 # g = .280
 q = 160

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION RUNS 127, 128, 129																					
SYMMETRIC MOTION																					
	ω''	ω'	ω	y''	y'	y	θ'	θ	α'	α	β''	β'	β	ρ''	ρ'	ρ	β''	β'	β	$F.F.$	
Eq. 1	.0225	.0265	.0094	.0104	.0172	-.1411	-22.217	-.0001	-.0197	-.2.998	.026	.0950	.1888	.4411	.6934	.7.211					
2	-.0172	-.0440	-.0319	-.0403	4.93	6.55	18.64	.1365	.66	9.38	-.2155	-.2365	-.686	-.1490	-.2.234	5.672					
3	.0463	.04872	.0839	.0887	-.1575	-.1998	-24.36	-.00821	-.1806	-22.26	.9335	.950	1.402	5.347	9.292	8.011					
4	.0025	.00310	.00468	.0045	.0182	-.0086	-.0110	-.1.457	-.0005	-.0099	-.1.237	.0463	.0444	.0779	.2040	.3302	.3511				
5	-.0025	-.00310	-.00468	-.0045	-.0047	.0032	.0057	.1980	.458	.0958	.1797	4.669	-.0472	-.0800	-.0512	-.0221	-.2.931				
ANTI-SYMMETRIC MOTION																					
	ϕ''	ϕ'	ϕ	y''	y'	y	α''	α'	α	β''	β'	β	ρ''	ρ'	ρ	β''	β'	β	$F.F.$		
Eq. 1	48.66	98.75	.845	1.198	-.0791	-1.770	-221.0	8.46	16.30	13.91	19.78	65.66	159.0X								
2	4.23	3.55	.0893	.0887	-.0081	-.1.895	-.22.25	.934	.950	1.426	5.347	9.292	8.90X								
3	.2265	.2010	.0168	.0045	.0182	-.0005	-.0099	-.1.237	.0462	.0444	.0779	.2040	.3302	.5009X							
4	-.2345	-.0047	-.0032	.0058	.1797	4.669	-.0472	-.0800	-.0512	-.0221	-.2.241										

PREPARED
CHECKED
REVISED

Alt. = 20,000 ft. $V = 501 \text{ ft/sec}$
 W₈₄ = 35,000 # $a = .175 \text{ ft.}$
 W₂₉ = 105,000 # $g = .84$
 Q = 160

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 MODEL

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION RUNS 130, 131, 132																					
SYMMETRIC MOTION																					
ω'' ω' ω y'' y' y θ'' θ' θ α'' α' α β'' β' β γ'' γ' γ ρ'' ρ' ρ																					
Eq. 1	.0254	.0265	.0265	.0026	.0104	-.0172	-.1411	-.12.217	-.0009	-.01972	-.2.998	.0926	.0950	.1888	.4411	.6934	.-7.211				
2	-.0172	-.0240	-.0240	-.0319	-.0403	5.745	6.55	18.04	1.945	.426	9.38	-.3155	-.3965	-.686	-.4.90	-.1.490	-2.294	5.478			
3	.0463	.04872	.04872	.0893	.0887	-.1575	-.1998	-.24.36	-.0081	-.1806	-.22.25	.9335	.950	1.402	5.347	9.292	8.018				
4	.0025	.00310	.00310	.01668	.0182	-.0086	-.0110	-.2.457	-.005	-.0099	-.1.237	.0463	.0644	.0779	.20.0	.3302	.3511				
5	-.0025	-.0047	-.0047	-.0032	.0957	.1980	.458	.0958	.1797	4.669	-.0471	-.0800	-.0512	-.0221	-.2391						
ANTI-SYMMETRIC MOTION																					
ω'' ϕ' ψ' y'' y' y α'' α' α β'' β' β γ'' γ' γ ρ'' ρ' ρ																					
Eq. 1	50.0	98.75	84.5	1.198		-.0791	-.1.770	-.221.0	8.46	16.30	13.91	39.78	65.66	159.0							
2	4.23	3.55	.0893	.0887		-.0081	-.1.895	-.22.25	.934	.950	1.402	5.347	9.292	8.90							
3	.2265	.2010	.00468	.0182		-.0005	-.0099	-.1.237	.0462	.0444	.0779	.20.0	.3302	.5009							
4	-.2345	-.2345	-.0047	.0032		.0958	.1797	4.669	-.0471	-.0800	-.0512	-.0221	-.2391								

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Alt. = 20,000 ft. $V = 354 \text{ ft/sec}$
 TBL = 11,500 ft. $a = .175 \text{ ft.}$
 N29 = 90,000 ft. $g_{\text{SL}} = .280$
 q = 80

DRAWN _____
 CHECKED _____
 REVISED _____

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TABLE II EQUATIONS OF MOTION											
COEFFICIENTS OF MOTION											
SYMMETRIC MOTION											
	1	2	3	4	5	6	7	8	9	10	11
	α'	α''	β'	β''	θ'	θ''	ϕ'	ϕ''	δ'	δ''	γ'
Eq. 1	.0438	.03452	.0165	.01669	-.0304	-.1982	-.12.217	-.0016	-.02791	-.2.998	.1633
2	.0304	.06220	.0562	.05689	9.81	9.252	18.64	.3824	.6017	9.38	-.5561
3	.0817	.06396	.1570	.1521	-.278	-.2.825	-.2.36	-.0123	-.2557	-.22.25	1.629
4	.0045	.004247	.0082	.006410	.0064	-.00122	-.001542	-.1.457	-.0008	-.01336	-.1.237
5	.003503	.005732	.0064	.0085	.0085	.2797	.463	.1.985	.2.534	.8.823	-.0664
	12	13	14	15	16	17	18	19	20	21	
	α'	α''	β'	β''	θ'	θ''	ϕ'	ϕ''	δ'	δ''	γ'
Eq. 2	87.73	339.7	1.491	1.691	-.1399	-.2.500	-.22.0	14.91	23.02	13.91	39.785
2	7.45	5.025	1.1570	1.1251	-.0143	-.2.557	-.22.25	1.629	1.343	1.402	5.347
3	.400	.2839	.0082	.006410	.0364	-.0008	-.01336	-.1.237	.0817	.06288	.0779
4	.3311			.006732	.0064	.1885	.2.534	.8.823		-.06641	-.0800
	12	13	14	15	16	17	18	19	20	21	
	α'	α''	β'	β''	θ'	θ''	ϕ'	ϕ''	δ'	δ''	γ'
Eq. 3	1	2	3	4	5	6	7	8	9	10	11
	α'	α''	β'	β''	θ'	θ''	ϕ'	ϕ''	δ'	δ''	γ'
Eq. 4											

ANTI-SYMMETRIC MOTION											
COEFFICIENTS OF MOTION											
ASYMMETRIC MOTION											
	1	2	3	4	5	6	7	8	9	10	11
	α'	α''	β'	β''	θ'	θ''	ϕ'	ϕ''	δ'	δ''	γ'
Eq. 1											
2											
3											
4											

W84	40,000 ft.	a	1/Sec
W84	11,500 #	a	.175 ft.
W29	120,000 #	c884	.280
		80	
		9	

PREPARED _____
CHECKED _____

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COEFFICIENTS OF EQUATIONS OF MOTION.

CONFERENCE

E-1-121

It.	= 20,000 ft.	V	= 134 ft/sec
34	= 11,500 #	a	= .175 ft.
29	= 90,000 #	984	= .280
22	= 120		

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Alt. = 20,000 ft. V = 434 ft/sec
 W₄ = 11,500 lb A = 2175 ft
 W₉ = 105,000 lb g₂₄ = .280
 q = 120

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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF EQUATIONS OF MOTION																					
RNS 143,140,150																					
SYMMETRIC MOTION																					
	W"	W'	W	y"	y'	y	θ"	θ'	θ	θ'	θ	θ"	θ'	θ	θ'	θ	θ"	θ'	θ	θ'	
R ₁ 1	.09312	.02815		.0110	.0110		-.0203	-.1625	12.217	.0010	-.00276	-2.998	.1088								
2	.02026	-.05073		-.0374	-.04660		7.612	7.546	18.64	.2549	.4908	9.38	-.3706	-.4570	6.295X						
3	.05444	.05624		.1047	.1021		-.1853	-.2304	-.2436	-.0095	-.2085	-.22.25	1.085	1.085	9.230X						
4	.00310	.003366		.00555	.005228		.02125	-.0101	-.01258	-.1457	-.0005	-.01138	-1.237	.0544	.05129	.4055X					
5	-.002857						.00244	.1256	.2283	.461	.1256	.2067	6.052		-.05417	-.3387X					
ANTI-SYMMETRIC MOTION																					
	Φ'	Φ	Φ	y"	y'	y	θ"	θ'	θ	θ'	θ	θ"	θ'	θ	θ'	θ	θ"	θ'	θ	θ'	
R ₁ 1	60.28	113.9		.994	1.379		-.0933	-2.039	-221.0	9.938	18.178	183.0X									
2	4.97	4.099		.1047	.1021		-.0095	-.2085	-.22.25	1.085	1.095	10.24X									
3	.266	.2316		.00555	.005228		.02125	-.0005	-.01138	-.1.237	.0544	.05129	.5782X								
4		-.2709					-.005190	.004244	.1256	.2067	6.052		-.05417	-.2577X							

Alt.	20,000 ft.	V	501 ft/sec.
#84	11,500 ft.	a	.175 ft.
#29	90,000 ft.	cg84	.280
	160		
	9		

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TABLE II-D
COEFFICIENTS OF EQUATIONS OF MOTION
RUNS #154, 155, 156

GONPHIENH

PREPARED _____
CHECKED _____

Alt.	20,000 ft.	500 ft/sec
W24	11,500 ft	a. 275 ft.
W29	10,500 ft	0g84 .280
q	160	

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**COEFFICIENTS OF EQUATIONS OF MOTION
RUNS # 51, 158, 159**

PREPARED
CHECKED
REVISED

Alt. = 35,000 ft. V = 465 ft/sec
W84 = 14,500 lb. a = 175 ft.
W29 = 90,000 lb. cE84 = .280
q = .80

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C	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

COEFFICIENTS OF EQUATIONS OF MOTION.

RUN # 163, 164, 165

L	ω	ϕ	ψ	θ	α	β	γ	α'	β'	γ'	α''	β''	γ''	α'''	β'''	γ'''	α''''	β''''	γ''''	α'''''
Eq. 1	.04619	.0263	.0079	.0122	.03831	-.1517	-12.217	-.00197	.0022	2.998	.2059	.1022	.1888	.4411	.6924	.9551				
2	-.03831	-.0474	-.0079	-.0433	.2.925	7.04	13.64	.4267	.458	9.38	-.7010	-.427	-.686	-.1.490	-.2.294	7.284				
3	.10289	.0525	.0991	.0353	-.3505	.215	-.24.36	-.01801	-.1946	-.22.25	2.079	1.022	1.02	5.347	9.292	10.421				
4	.00563	.0031	.0104	.0049	.0364	-.01915	-.0117	-.3.657	-.000984	-.0106	-.1.237	.1029	.0479	.0779	.2042	.4551				
5	-.0027	-.0051	.0064	.2100	.2129	.461	.2100	.1929	8.823	-.0206	-.0010	-.0512	-.0224	-.3831						

ANTI-SYMMETRICAL MOTION

L	ϕ	ψ	θ	α	β	γ	α'	β'	γ'	α''	β''	γ''	α'''	β'''	γ'''	α''''	β''''	γ''''	α'''''	
Eq. 1	10.65	106.3	1.882	1.287	-.1764	-.1.903	-22.0	18.85	17.52	13.31	39.785	65.66	222.91							
2	9.449	3.80	.1991	.0953	-.01801	-.1946	-.22.25	2.079	1.022	1.402	5.347	9.292	12.471							
3	.5040	.2161	.0104	.0049	-.000984	-.0106	-.1.237	.1029	.0479	.0779	.2042	.3302	.7041							
4	-.252	-.0051	.0064	.2100	.1929	8.823	-.0506	-.0800	-.0512	-.0224	-.3141									

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PREPARED
CHECKED
REVISED

Alt. 35,000 ft. V = 465 ft./sec.
W₈₄ = 14,500 ft. a = 175 ft.
W₂₉ = 105,000 q = .280
q = 80

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	1	2.	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

TABLE II-D
COEFFICIENTS OF MOTION
RUNS 156, 157, 168

STILLERICAL MOTION

	W ₁	W ₂	W ₃	Y ₁	Y ₂	Y ₃	θ ₁	θ ₂	θ ₃	X ₁	X ₂	X ₃	Y ₁	Y ₂	Y ₃	θ ₁	θ ₂	θ ₃	F.F.	
Eq. 1	.0520	.0263	.02079	.0112	.03831	-.1517	-.22.217	.00197	.0012	.2659	.18.98	.1022	.1888	.4411	.6924	.9.551				
2	-.03821	.0474	.07079	-.0633	11.488	7.04	18.64	.4267	.458	9.38	-.7010	-.127	-.686	-.1.490	-.2.224	7.284				
3	.1029	.0525	.11921	.0953	-.3505	-.2115	-.24.36	-.01801	-.1946	-.22.25	2.079	1.022	1.402	5.347	9.292	10.421				
4	.00563	.0321	.0104	.0049	.0364	-.01915	-.0117	-.01457	-.000984	-.0106	-.1.237	.1029	.0479	.0779	.2041	.3202	.4552			
5	-.0027			-.0051	.0064	.2100	.2129	.461	.2100	.1929	8.823	-.0506	-.0800	-.0512	-.0224	-.3828				

ANTI-STILLERICAL MOTION

	W ₁	W ₂	W ₃	Y ₁	Y ₂	Y ₃	θ ₁	θ ₂	θ ₃	X ₁	X ₂	X ₃	Y ₁	Y ₂	Y ₃	θ ₁	θ ₂	θ ₃	F.F.
Eq. 1	109.14	106.3	1.882	1.287	-.1764	-1.903	-2.21.0	18.85	17.32	13.91	39.785	65.66	222.95						
2	9.419	3.83	.1.991	.0953	-.01801	-.1946	-.22.25	2.079	1.022	1.402	5.347	9.292	12.472						
3	.5040	.2161	.0104	.0049	.0364	-.000984	-.0106	-.1.237	.1029	.0479	.0779	.2041	.3302	.7044					
4	-.252		-.0051	.0064	.2100	.1929	8.823	-.0506	-.0800	-.0512	-.0224	-.3144							

1lt.	$\frac{35,000}{\$84}$	Y	$\frac{465}{\$84}$
	$\frac{14,500}{\$29}$	a	$\frac{175}{\$29}$
	$\frac{120,000}{\$84}$	cgs	$\frac{280}{\$84}$
	80	q	q

REMARKS

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MODEL

1305

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COEFFICIENTS OF TABLE II-V
EQUATIONS OF MOTION
RUNS* 162, 170, 171

卷之三

PREPARED
CHECKED
REVISED

Alt. = 35,000 ft. V = 520 ft/sec.
 Eq. = 14,500 ft. a = .175 ft.
 Eq. = 105,000 ft. c_{g04} = .280
 q = 100

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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
--	---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----

TABLE II - COEFFICIENTS OF EQUATIONS OF MOTION.

	SYMMETRICAL MOTION										ASYMMETRICAL MOTION										
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Eq. 1	.0416	.0235	.0163	.0100	.03065	.0356	.22.217	.00138	-.0190	-.2.998	-.1.647	.0914	.1888	.6411	.6924	.8.544					
2	-.03065	-.0423	-.05663	-.0387	9.190	6.298	18.64	.3.224	.4.096	9.38	.5.608	-.3.824	-.6.96	-.1.490	-.2.294	6.5111					
3	.08235	.0469	.1592	.0852	-.2.804	-.1.923	-.24.36	-.0.1641	-.1.740	-.22.25	1.663	.9.22	.1.402	5.247	9.22	9.3198					
4	.00450	.0028	.00032	.0044	.0251	-.01532	-.0105	-.1.457	-.0.00788	-.0095	-.1.237	.08235	.0.028	.0.0779	.2.041	.3.02	.4.088				
5	-.0024		-.0046	.0051	.1680	.1904	.461	.1.680	.1.725	.7.160		.0.452	-.0.0500	-.0.522	-.0.0224	-.3.31X					

SYMMETRICAL MOTION

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Eq. 1	87.31	95.07	1.506	1.151	-.1.411	-.1.702	-.221.0	15.08	15.67	13.91	39.785	65.66	199.3X								
2	7.536	3.42	.1593	.0852	-.01441	-.1740	-.22.25	1.663	.9.42	1.402	5.347	9.292	11.15X								
3	.4032	.1933	.00832	.0044	.0291	-.000788	-.0095	-.1.237	.08235	.0428	.0779	.2.041	.3.02	.6.30X							
4	-.2254		-.0046	.0051	.1680	.1.725	.7.160		-.0.452	-.0.0500	-.0.522	-.0.0224	-.2.81X								

ASYMMETRICAL MOTION

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Eq. 1	87.31	95.07	1.506	1.151	-.1.411	-.1.702	-.221.0	15.08	15.67	13.91	39.785	65.66	199.3X								
2	7.536	3.42	.1593	.0852	-.01441	-.1740	-.22.25	1.663	.9.42	1.402	5.347	9.292	11.15X								
3	.4032	.1933	.00832	.0044	.0291	-.000788	-.0095	-.1.237	.08235	.0428	.0779	.2.041	.3.02	.6.30X							
4	-.2254		-.0046	.0051	.1680	.1.725	.7.160		-.0.452	-.0.0500	-.0.522	-.0.0224	-.2.81X								

ANTI-SYMMETRICAL MOTION

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Eq. 1	87.31	95.07	1.506	1.151	-.1.411	-.1.702	-.221.0	15.08	15.67	13.91	39.785	65.66	199.3X								
2	7.536	3.42	.1593	.0852	-.01441	-.1740	-.22.25	1.663	.9.42	1.402	5.347	9.292	11.15X								
3	.4032	.1933	.00832	.0044	.0291	-.000788	-.0095	-.1.237	.08235	.0428	.0779	.2.041	.3.02	.6.30X							
4	-.2254		-.0046	.0051	.1680	.1.725	.7.160		-.0.452	-.0.0500	-.0.522	-.0.0224	-.2.81X								

SYMMETRICAL MOTION

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Eq. 1	87.31	95.07	1.506	1.151	-.1.411	-.1.702	-.221.0	15.08	15.67	13.91	39.785	65.66	199.3X								
2	7.536	3.42	.1593	.0852	-.01441	-.1740	-.22.25	1.663	.9.42	1.402	5.347	9.292	11.15X								
3	.4032	.1933	.00832	.0044	.0291	-.000788	-.0095	-.1.237	.08235	.0428	.0779	.2.041	.3.02	.6.30X							
4	-.2254		-.0046	.0051	.1680	.1.725	.7.160		-.0.452	-.0.0500	-.0.522	-.0.0224	-.2.81X								

ASYMMETRICAL MOTION

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Eq. 1	87.31	95.07	1.506	1.151	-.1.411	-.1.702	-.221.0	15.08	15.67	13.91	39.785	65.66	199.3X								
2	7.536	3.42	.1593	.0852	-.01441	-.1740	-.22.25	1.663	.9.42	1.402	5.347	9.292	11.15X								
3	.4032	.1933	.00832	.0044	.0291	-.000788	-.0095	-.1.237	.08235	.0428	.0779	.2.041	.3.02	.6.30X							
4	-.2254		-.0046	.0051	.1680	.1.725	.7.160		-.0.452	-.0.0500	-.0.522	-.0.0224	-.2.81X								

ANTI-SYMMETRICAL MOTION

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Eq. 1	87.31	95.07	1.506	1.151	-.1.411	-.1.702	-.221.0	15.08	15.67	13.91	39.785	65.66	199.3X								
2	7.536	3.42	.1593	.0852	-.01441	-.1740	-.22.25	1.663	.9.42	1.402	5.347	9.292	11.15X								
3	.4032	.1933	.00832	.0044	.0291	-.000788	-.0095	-.1.237	.08235	.0428	.0779	.2.041	.3.02	.6.30X							
4	-.2254		-.0046	.0051	.1680	.1.725	.7.160		-.0.452	-.0.0500	-.0.522	-.0.0224	-.2.81X								

SYMMETRICAL MOTION

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
Eq. 1	87.31	95.07	1.506	1.151	-.1.411	-.1.702	-.221.0	15.08	15.67	13.91	39.785	65.66	199.3X								
2	7.536	3.42	.1593	.0852	-.01441	-.1740	-.22.25	1.663	.9.42	1.402	5.347	9.292	11.15X								
3	.4032	.1933	.00832	.0044	.0291	-.000788	-.0095	-.1.237	.08235	.0428	.0779	.2.041	.3.02	.6.30X							
4	-.2254		-.0046	.0051	.1680	.1.725	.7.160		-.0.452	-.0.050											

at.	35,000 ft.	v	= 520 ft./sec.
4	24,500	a	= .175 ft.
9	120,000	c ₈₄	= .280
	100		

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Report No. 1

TABLE I
COEFFICIENTS OF EQUATIONS OF MOTION.
RUNS # 116, 117, 118

卷之三

Alt.	35,000 ft.	V	= 570 ft/sec
1884	14,500 ft.	a	= .175 ft.
1229	90,000 ft.	c _{B84}	= .280
		q	.120

PREFACE

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CONFIDENTIAL

**COEFFICIENTS OF EQUATIONS OF MOTION
RUNS * 18182183**

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION RUNS # 181, 182, 183																				
SYMMETRICAL MOTION																				
\dot{W}''	\dot{W}''	\dot{W}'	\dot{W}	\dot{Y}''	\dot{Y}'	\dot{Y}	$\dot{\Theta}''$	$\dot{\Theta}'$	$\dot{\Theta}$	\dot{x}''	\dot{x}'	\dot{x}	α''	α'	α	β''	β'	β	γ''	γ'
.03079	.0224	.01386	.0091	-.02554	-.02237	-.12.217	-.001131	-.0173	-.2.998	.0172	.0034	.1888	.4411	.6934	.4411	.6934	.7.7921			
-.02554	-.0286	-.04719	-.0353	6.617	5.764	18.64	.2845	.3736	9.38	-.4673	-.3479	-.6886	-.4690	-.2.294	5.9398					
.06863	.0428	.1128	.0777	-.2337.	-.1754	-.24.36	-.01201	-.1587	-.22.25	1.386	.8339	1.402	.5347	9.292	8.5011					
.00375	.0026	.00693	.0040	.0243	-.01277	-.0096	-.1.457	-.0087	-.1.237	.06863	.0390	.0779	.2041	.3302	.3701					
-.0022		-.0042		.0003	.1400	.1756	.461	.14.0	.1573	6.052		-.0412	-.0800	-.0512	-.0224	-.3321				
ANTI-SYMMETRICAL MOTION																				
ϕ''	ϕ'	ϕ	ψ''	ψ'	ψ	α''	α'	α	β''	β'	β	γ''	γ'	γ	δ''	δ'	δ	ϵ''	ϵ'	ϵ
70.97	86.72	1.255	1.050	-.1176	-.1.552	-.221.0	12.57	14.29	13.91	39.785	65.66	181.72								
6.280	3.12	.1328	.0777	-.01201	-.1587	-.22.25	1.386	.8339	1.402	5.347	9.292	10.172								
.3360	.1762	.00693	.3040	.0243	-.000656	-.3087	-.1.237	.06863	.0390	.0779	.2041	.3302	.5742							
-.206		-.2042		.0003	.1400	.1573	6.052		-.0412	-.0800	-.0512	-.0224	-.2561							

CONTINUOUS

卷之四

PREPARED _____
CHECKED _____
REVISED _____

Wt. = 33,500 lb. V = 570 ft./sec
W29 = 14,500 lb. A = .75 ft.
W29 = 105,000 lb. Q = .884 ft.
q = 140

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

COEFFICIENTS OF EQUATIONS OF MOTION
RUNS 104, 105, 106

SYMMETRICAL MOTION

	ω'	ω''	y'	y''	θ'	θ''	α'	α''	β'	β''	γ'	γ''	α'	α''	β'	β''	γ'	γ''
Eq. 1	.03467	.0214	.01386	.0091	-.02554	-.1237	-.12.217	-.00131	-.0173	-.2.998	.137	.0836	.1888	.4411	.6934	.7.7921		
2	-.02554	-.0386	-.04719	-.0353	7.659	5.744	18.64	.2845	.3736	9.38	-.4673	-.3479	-.686	-1.490	-2.294	5.9293		
3	.06863	.0428	.1328	.0777	-.2337	-.1754	-.24.36	-.01201	-.1587	-.22.25	1.386	.8339	1.402	5.347	9.292	8.5011		
4	.00375	.0026	.00693	.0040	.0242	-.01277	-.0096	-.1.457	-.000656	-.0087	-.1.237	.06863	.0390	.0779	.2041	.3302	.3701	
5	-.0022	-.0042	-.0043	.0043	.2400	.1736	.461	.2400	.1573	.6.052				-.0412	-.0800	-.0512	-.0224	-.2131

ANTI-SYMMETRICAL MOTION

	ϕ'	ϕ''	ψ'	ψ''	y'	y''	α'	α''	β'	β''	γ'	γ''	α'	α''	β'	β''	γ'	γ''
1	.72.76	86.72	1.255	1.950	-.1176	-.1.582	-.221.0	12.57	14.29	13.91	.39.785	65.66	181.72					
2	6.280	3.12	.1328	.0777	-.01201	-.1.587	-.22.25	1.386	.8339	1.402	5.347	9.292	10.171					
3	.3360	.1762	.00693	.0040	.0243	-.000656	-.0087	-.1.237	.06863	.0390	.0779	.2041	.3302	.5741				
4	-.206	-.0042	-.0043	.0043	.2400	.1736	.461	.2400	.1573	.6.052	-.0412	-.0800	-.0512	-.0224	-.2561			

E-1-129
SER 1/6/94

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PREPARED
CHECKED
REVISED

Alt. = 35,000 ft. V = 570 ft./sec.
W₈₄ = 14,500 lb a = 175 ft.
W₂₉ = 120,000 lb g₈₄ = .280
q = 120

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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION RUNS 187, 188, 189																					
STATIONARY MOTION																					
α' ω' ψ' $\dot{\alpha}'$ $\dot{\omega}'$ $\dot{\psi}'$																					
α'' ω'' ψ'' $\dot{\alpha}''$ $\dot{\omega}''$ $\dot{\psi}''$																					
θ' θ''																					
β' β''																					
γ' γ''																					
$\alpha = 0$ $\alpha = 1.5$ $\alpha = 3.0$																					
$\beta = 0$ $\beta = 1.5$ $\beta = 3.0$																					
$\gamma = 0$ $\gamma = 1.5$ $\gamma = 3.0$																					

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
ANTI-SYMETRICAL MOTION																					
α' ω' ψ' $\dot{\alpha}'$ $\dot{\omega}'$ $\dot{\psi}'$																					
α'' ω'' ψ'' $\dot{\alpha}''$ $\dot{\omega}''$ $\dot{\psi}''$																					
θ' θ''																					
β' β''																					
γ' γ''																					
$\alpha = 0$ $\alpha = 1.5$ $\alpha = 3.0$																					
$\beta = 0$ $\beta = 1.5$ $\beta = 3.0$																					
$\gamma = 0$ $\gamma = 1.5$ $\gamma = 3.0$																					

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Alt. = 35,000 ft. V = 465
 W_A = 13,000 # a = .175 ft.
 W₂₉ = 90,000 # c_B = .280
 q = 80

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 [CONFIDENTIAL]

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
	COEFFICIENTS OF EQUATIONS OF MOTION RUNS 1 TO 11, 192																				
	SIMILARITY MOTION																				
	ANTI-SYMMETRIC MOTION																				
	W"	W'	W"	Y"	Y'	Y"	Φ'	Φ"	θ'	θ"	θ'	θ"	α'	α"	β'	β"	γ'	γ"	δ'	δ"	F.F.
Eq. 1	.04504	.02628	.01866	.01118	.01118	.01118	.01118	.01118	-.03139	-.03139	-.03139	-.03139	-.15156	-.12.217	-.001768	-.02125	-.2.938	.18.8	.1022	-.9.554	
2	-.03139	-.04735	-.06354	-.04231	-.04231	-.04231	-.04231	-.04231	9.83	7.043	7.043	7.043	18.64	23.82	.4580	9.38	-.6233	-.4266	7.281	10.42	
3	.09241	.05249	.01787	.09227	.09227	.09227	.09227	.09227	-.31.47	-.21.50	-.21.50	-.21.50	-.24.36	-.21.617	-.1946	-.22.25	1.865	1.022	.09241	.05056	
4	.005050	.003112	.009332	.004380	.006388	.006388	.006388	.006388	-.01175	-.01175	-.01175	-.01175	-.1.457	-.0088398	-.01062	-.1.237	.09242	.04787	.04787	.05056	
5	-.002672			-.005125	.006366	.006366	.006366	.006366	.1916	.2129	.2129	.2129	.4610	.1916	.1920	8.823	-.05056	-.3834	-.3834		

Eq. 1 97.26 106.3 8.455 3.826 3.425 .2161 -.2.521
 2 8.455 3.826 3.425 .2161 -.2.521
 3 3.425 .2161 1.878 .04527 .009332 .004879 -.005126
 4 .2161 -.2.521

[CONFIDENTIAL]

Alt.	35,000 ft.	V	465
W84	13,000 ft.	a	.175 ft.
W29	105,000 ft.	cg	.280
g	80		

EXERCISES
PREPARED

CONFIDENTIAL EDR-C-205-104

CONFIDENTIAL

$\Delta t = 35,000 \text{ sec}$. $V \text{ ft/sec} = 465$
 $R_4 = 13,000 \text{ ft}$. $a = 1.75 \text{ ft.}$
 $R_2 = 120,000 \text{ ft}$. $g_{684} = .280$
 $q = 80$

PREPARED
CHECKED
REVIEWED

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
--	---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----

TABLE II-D
COEFFICIENTS OF EQUATIONS OF MOTION
RUNS 196, 197, 198

	w_1	w_2	y_1	y_2	θ_1	θ_2	α_1	α_2	β_1	β_2	γ_1	γ_2	δ_1	δ_2	ϵ_1	ϵ_2	ζ_1	ζ_2	ϕ_1	ϕ_2	
Bq. 1	.05670	.02628	.01866	.01118	-.03429	-.1516	-.12.217	-.001768	-.001225	-.2.998	.1848	.1022	.1888	.4411	.6934	.4411	.6934	.-9.5541			
2	-.03439	-.06735	-.06354	-.0531	13.00	7.023	18.64	.680	.3892	9.38	-.6293	-.4266	-.6860	-.1.690	-.2.294	-.1.690	-.2.294	7.2811			
3	.03441	.03249	.03877	.03527	-.3147	-.2150	-.24.36	-.01617	-.1946	-.22.25	1.865	1.022	1.402	1.347	9.232	10.422					
4	.03550	.03142	.03932	.03638	-.004820	.03638	-.01720	-.01175	-.01457	-.00838	-.01062	-.1.237	-.09242	-.04787	.0779	.2042	.3102	.4549			
5	-.032672	-.032672	-.005125	.006366	.1916	.2129	.4610	.1916	.1916	.1916	.1916	.1916	.1916	.1916	-.05056	-.07992	-.05118	-.07244	-.38341		

ANTI-SYMMETRIC MOTION

	α_1	α_2	β_1	β_2	γ_1	γ_2	δ_1	δ_2	ϵ_1	ϵ_2	ζ_1	ζ_2	ϕ_1	ϕ_2	ψ_1	ψ_2	χ_1	χ_2	ρ_1	ρ_2	
Bq. 1	102.5	106.3	1.030	1.287	-.1524	-.1.903	-.21.0	16.32	17.52	13.91	39.79	65.66	222.8								
2	8.455	3.826	.1787	.29527	-.01617	-.1.946	-.2.25	1.865	1.022	1.412	5.347	9.292	12.46								
3	4.525	.2161	.007332	.004870	.03638	.0008837	-.01062	-.1.237	.09241	.04787	.0779	.2041	.3302	.7038							
4	-.2521		.09126	.006366	.1916	.1916	.1916	.1916	.1916	.1916	-.05056	-.07992	-.05118	-.07244	-.3137						

CONFIDENTIAL

REPAIRED _____
CHECKED _____
INSPECTED _____

1st.	\$ 35,000 R.
2nd.	\$ 13,000 R.
3rd.	\$ 90,000 R.
4th.	\$ 100.
	V = \$20
	a = .1751 C.Q. = .280

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	ϕ	ψ	θ	α	β	γ	δ	ϵ	ζ	η	ξ	ζ	η	ξ
1	.77.70	95.06		1.352	2.151		-.1267	-1.702	-221.0	13.54		15.67		
2	6.764	3.621		.1430	.08519		-.01294	-.1740	-22.25	1.442		.9140		
3	.3620	.1922		.007466	.004363	.002320	-.0007070	-.0059497	-.1.237	.0739		.04281		
	.2254			.004584	.0001082	.15313		.1724		7.160			-.04522	

5-1-12

Alt. = 35,000 ft.	V ft/sec = 520
184 = 15,000 ft	a = .175 ft.
229 = 120,000 ft	C.G. = .280
= 100	

PREPARED
CHECKED
REVISED

CONFIDENTIAL - ECR-0005-104

REPAVED
CHECKED
UNWISED

COEFFICIENTS OF EQUATIONS OF MOTION												
SYMMETRIC MOTION												
RUNS # 205, 206, 207												
1	2	3	4	5	6	7	8	9	10	11	12	
ω_1	ω_2	ω_3	ω_4	ω_5	ω_6	ω_7	ω_8	ω_9	ω_{10}	ω_{11}	ω_{12}	
.04536	.02150	.01493	.01000	-.02751	-.1336	-12.217	-.001424	-.01900	-2.298	.2678	.09139	
1	2	3	4	5	6	7	8	9	10	11	12	
-.02751	-.04234	-.05084	-.03873	10.40	6.298	18.64	.3114	-.0096	9.38	-.5024	-.3815	
3	4	5	6	7	8	9	10	11	12	13	14	
.07393	.0664	.007466	.004263	.02910	-.01376	-.01051	-.1.457	-.0007070	-.009498	-.2.237	.07394	
4	5	6	7	8	9	10	11	12	13	14	15	
.004263	.002810	-.004583	.005092	.1533	.1904	.4610	.1533	.1725	.7.160	-.04521	-.07992	
5	6	7	8	9	10	11	12	13	14	15	16	
-.002388	-.002388	-.004583	.005092	.1533	.1904	.4610	.1533	.1725	.7.160	-.04521	-.07992	
6	7	8	9	10	11	12	13	14	15	16	17	
-.002388	-.002388	-.004583	.005092	.1533	.1904	.4610	.1533	.1725	.7.160	-.04521	-.07992	-.05118
7	8	9	10	11	12	13	14	15	16	17	18	
-.002388	-.002388	-.004583	.005092	.1533	.1904	.4610	.1533	.1725	.7.160	-.04521	-.07992	-.05118
8	9	10	11	12	13	14	15	16	17	18	19	
-.002388	-.002388	-.004583	.005092	.1533	.1904	.4610	.1533	.1725	.7.160	-.04521	-.07992	-.05118
9	10	11	12	13	14	15	16	17	18	19	20	
-.002388	-.002388	-.004583	.005092	.1533	.1904	.4610	.1533	.1725	.7.160	-.04521	-.07992	-.05118
10	11	12	13	14	15	16	17	18	19	20	21	
-.002388	-.002388	-.004583	.005092	.1533	.1904	.4610	.1533	.1725	.7.160	-.04521	-.07992	-.05118

CONFIDENTIAL

PREPARED
CHECKED
REVISED

$\Delta t = 35,000$ 1 $V = 570$
 $\frac{W_A}{W} = 13,000$ 1 $\alpha = .175$
 $\frac{W_2}{W} = 90,000$ 1 $O.A. = .280$
 $\theta = 120^\circ/\text{sec}^2$

CONFIDENTIAL

NOTE - 4905-504
NOTE

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF EQUATIONS OF MOTION.																					
RUNS # 208 209 210																					
	ω	ω	α	α	β	β	θ	θ	α	α	β	β	θ	θ	α	α	β	β	θ	θ	
Eq. 1	.03002	.08144	.009120	.002444	-.002993	-.1237	-.12217	-.002179	.01734	-.2,98	.1232	.08337									
2	-.02293	-.03863	-.04236	.03537	6.584	5.746	18.64	.2595	.3736	9.38	-.4195	-.3480									
3	.06161	.04282	.1191	.07772	-.2098	-.1754	-.24.36	-.01078	-.1588	-.77.75	1.243	.8337									
4	.003367	.002563	.006221	.003281	.02246	-.01147	-.009285	-.1457	-.000582	-.000561	-.1.237	.06161	.03905								
5	-.002180				-.002181	.00244	.2277	.1737	.4610	.3277	.1574	6.052	-.04224								

ANTI-SYMMETRIC MOTION

	α	β	α	β	α	β	α	β	α	β	α	β	
1	57.36	86.72	1.127	1.050	-.1056	-.1.552	-.221.0	11.28	14.29				
2	5.637	3.121	.1191	.07772	-.01078	-.1588	-.22.25	1.243	.8337				
3	.3017	.1763	.006221	.003280	.02425	-.000582	-.008664	-.1.237	.06161	.03905			
4	-.2056				-.004182	.00244	.2277	.1574	6.052	-.04224			

CONFIDENTIAL

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EDR-C905-104

Alt. = 35,000 ft. V = 570
W₆ = 13,000 # A = 1.175
W₉ = 105,000 # C.G. = .280
G = 120

PREPARED
CHECKED
REVISED

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
--	---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----

TABLE II - COEFFICIENTS OF EQUATIONS OF MOTION.
RUNS 211, 212, 213.

SIMMETRIC MOTION

	ω'	ω	ψ'	ψ	θ'	θ	χ'	χ	α'	α	β'	β	γ'	γ	ζ'	ζ	ξ'	ξ	η'	η	
R ₁ 1	.03390	.02244	.00920	.00293	-	-0.237	-12.217	-	.001179	-	.01734	-	.2988	-	.2232	-	.08337	-	.738	-	
2	-.02293	-.02363	-.03533	-.04236	7.625	15.746	18.66	.2595	.3736	9.38	.4495	.3480	.4495	.3480	.5940	.5940	.5940	.5940	.5940	.5940	
3	.06161	.04282	.01921	.00772	-.2096	-.1754	-.24.36	-.01078	-.1588	-.22.25	1.243	8.337	1.243	8.337	8.500	8.500	8.500	8.500	8.500	8.500	
4	.003367	.002563	.0006221	.003981	.002425	-.01147	-.009585	-.1.457	-.0005892	-.008664	-.1.237	.06161	.03905	.06161	.03905	.3711	.3711	.3711	.3711	.3711	.3711
5	-.002180	-.002181	-.002181	-.002181	.004244	.1277	.1737	.4610	.1277	.1574	6.032	-.04124	6.032	-.04124	6.032	-.3128	-.3128	-.3128	-.3128	-.3128	-.3128

ANTI-SYMMETRIC MOTION

	Φ'	Φ	ψ'	ψ	θ'	θ	χ'	χ	α'	α	β'	β	γ'	γ	ζ'	ζ	ξ'	ξ	η'	η
R ₁ 1	66.56	86.72	1.127	1.050	-.1056	-1.552	-221.0	11.28	14.29	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8	181.8
2	5.637	3.121	.1191	.07772	-.01078	-.1.588	-.22.25	1.243	.8337	.8337	.8337	.8337	.8337	.8337	.8337	.8337	.8337	.8337	.8337	.8337
3	.3017	.1763	.006221	.003980	.004245	-.0005892	-.008664	-.1.237	.06161	.03905	.06161	.03905	.06161	.03905	.06161	.03905	.06161	.03905	.06161	.03905
4	-.2056	-.004182	-.004244	-.004244	.1277	.1574	.6.032	-.04124	-.04124	-.04124	-.04124	-.04124	-.04124	-.04124	-.04124	-.04124	-.04124	-.04124	-.04124	-.04124

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Alt. = 35,000 ft. V = 465 ft/sec
Max. = 11,500 ft. = .175 ft.
R29 = 90,000 ft. 0.004 = .280
q = 80

REF ID: A65152204
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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF EQUATIONS OF MOTION																					
RUNS # 217, 218, 219																					
SYMMETRIC MOTION																					
Bx. 1	.0439	.0863	.0165	.0112	.0112	.0804	.1517	.3217	-.0016	-.2212	2.998	.1633	.0200	.0888	.4411	.0694	.9551				
2	-.0304	-.0474	-.0532	-.0433	9.856	7.04	18.64	.3824	.458	9.38	-.5561	-.427	-.686	-.490	-2.294	7.281					
3	.0817	.0525	.1570	.0953	-.278	-.215	-.26.36	-.0213	-.1946	-.22.25	1.629	1.022	1.402	5.347	9.292	10.424					
4	.0045	.0031	.0032	.0364	-.0152	-.0117	-.1.457	-.0008	-.0106	-.1.237	.0817	.0479	.0779	.2041	.3302	.4551					
5	-.0027			-.0051	.0066	.1885	.2129	.461	.1885	.1885	.1829	.0506	-.0800	-.0312	-.0224	-.3831					
ASYMMETRIC MOTION																					
Bx. 1	87.73	106.3	1.491	1.287																	
2	7.45	3.83	.1570	.0953																	
3	.400	.2161	.0082	.0049																	
4	-.252			-.0051	.0066																

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	Alt.	W84	W29	W29	W84
	35,000 ft.	V	V	V	V
	11,500 ft.	A	A	A	A
	105,000 ft.	C	C	C	C
q	80				

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6 AUG

TABLE II-D
COEFFICIENTS OF EQUATIONS OF MOTION
RUNS # 220 221 222

WITI-SYMMETRIC MOTION

	Φ^+	Φ^-	Ψ^+	Ψ^-	α''	α'	α	β''	β'	β	F_β	
1	.9042	106.3	1.491	1.287	-.1399	-1.903	-221.0	14.91	17.52	13.91	39.785	65.66
2	7.45	3.83	.1570	.0953	-.0143	-.1946	-22.25	1.629	1.022	1.02	5.347	9.292
3	.400	.2161	.0082	.0049	.0364	-.0008	-.0106	-.1.237	.0817	.0479	.0779	.2041
4	-.232		-.0051	.0064	.1885	.1929	.8.823		-.0506	-.0800	-.0512	-.0224

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REVISU

Airs. = 35,000 ft. V = 465 ft/sec
M24 = 11,500 # S = .175 ft.
M29 = 120,000 # C.G. 84 = .280
q = 80

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CONFIDENTIAL - EDR-C905-104

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF EQUATIONS OF MOTION																					
RUNS 223, 224, 225																					
SYMMETRIC MOTION																					
	$\dot{\omega}$	\dot{w}	\dot{y}	\dot{y}'	\dot{y}''	θ	θ'	θ''	α	α'	α''	β	β'	β''	γ	γ'	γ''	δ	δ'	δ''	
Eq. 1	.05553	.0263	.0112	.0165	.0112	-.0304	-.1527	-.12217	-.0016	-.0212	-.2998	.1633	.1022	.1688	.4411	.6924	.22.52				
2	-.0304	-.0474	-.0433	-.0582	-.0433	12.98	7.04	18.64	.3824	.458	9.38	-.5561	-.427	-.686	-.1.490	-.2.294	-.7.281				
3	.0817	.0525	.0953	.1570	.0953	-.278	-.215	-.24.36	-.0143	-.1946	-.22.25	1.629	1.022	1.602	.5347	.9.292	10.421				
4	.0045	.0031	.0049	.0082	.0049	.0364	-.0117	-.0157	-.0008	-.0106	-.1.237	.0817	.0479	.0779	.20.21	.3202	.4552				
5	-.0027					-.0051	.0064	.1885	.2129	.461	.1885	.1929	.8.823	-.0506	-.0800	-.0512	-.0824	-.3831			
ANTI-SYMMETRIC MOTION																					
	$\dot{\Phi}$	$\dot{\phi}$	\dot{y}'	\dot{y}''	y	y'	y''	α'	α''	β'	β''	β	β'	β''	γ	γ'	γ''	δ	δ'	δ''	
Eq. 1	93.07	106.3	1.491	1.287				-.1399	-.1.903	-.221.0	14.91	17.52	13.91	39.785	65.66	22.52					
2	7.45	3.83	.1570	.0953				-.0143	-.1946	-.22.25	1.629	1.022	1.402	5.347	9.292	12.471					
3	.400	.2161	.0082	.0049				-.0008	-.0106	-.1.237	.0817	.0479	.0779	.20.21	.3302	.7042					
4	-.252		-.0051	.0064				.0064	.1885	.1929	.8.823	-.0506	-.0800	-.0512	-.0824	-.3141					

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Alt.	= 35,000 ft.	V	= 320 ft./sec.
W84	= 11,500 ft.	a	= 175 ft.
R29	= 90,000 ft.	c.g.-84	.280
	= 100		
		q	

PREPARED _____
CHECKED _____
REVIEWED _____

CONFIDENTIAL

COEFFICIENTS OF EQUATIONS OF MOTION
RUNS # 246, 227, 228

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$$\begin{aligned}
 \text{Alt} &= 35,000 \text{ ft.} & V &= 520 \text{ ft/sec} \\
 W_{84} &= .11500\% & a &= 175 \text{ ft.} \\
 W_{29} &= 105,000\% & \text{Cn84} &= .280
 \end{aligned}$$

$$W_{84} = 11 \\ W_{29} = 10$$

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CHECKED
REVISED

Alt = 35,000 ft. V = 520 ft/sec
 $\frac{V^2}{q} = 115000$ ft. a = .175 ft.
 $\frac{V^2}{q} = 120,000$ ft. C.G.S. = .280
 $q = 100$

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[CONFIDENTIAL]

		TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION											
		RUNS 232, 233, 234											
		SYMMETRICAL MOTION											
A	B	C	D	E	F	G	H	K	L	M	N	O	P
1	2	3	4	5	6	7	8	9	10	11	12	13	14
2	3	4	5	6	7	8	9	10	11	12	13	14	15
3	4	5	6	7	8	9	10	11	12	13	14	15	16
4	5	6	7	8	9	10	11	12	13	14	15	16	17
5	6	7	8	9	10	11	12	13	14	15	16	17	18
6	7	8	9	10	11	12	13	14	15	16	17	18	19
7	8	9	10	11	12	13	14	15	16	17	18	19	20
8	9	10	11	12	13	14	15	16	17	18	19	20	21

[CONFIDENTIAL]

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Alt = 25,000 ft. V = 570 ft/sec
 V₈₄ = 11500 ft. a = .175 ft.
 V₂₉ = 20,000 ft. C.G. g₄ = .260
 q = 120



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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
A	B	C	D	E	F	G	H	I	J	K	L	M	N	O	P	Q	R	S	T	U	V
TABLE II-P COEFFICIENTS OF EQUATIONS OF MOTION RUNS 235, 236, 237 SYMMETRICAL MOTION																					
α'																					
1	.0292	.0214	-	-.0110	.0091	-	-.0203	-.1237	-.12.21	-.0010	-.0173	-2.998	-.1038	.0834	.1888	.4411	.6934	-7.7923			
2	-.0203	-.0386	-	-.0374	-.0353	-	6.568	5.744	18.64	.2549	.2036	9.38	-.3706	-.3479	-.686	-.1490	-2.894	5.939			
3	.0544	.0428	-	.1047	.0777	-	-.1353	-.1754	-.24.36	-.0095	-.1587	-22.25	1.085	.8339	1.402	5.347	9.292	8.501			
4	.0030	.0026	-	.0055	.0040	.0243	-.0101	-.0096	-.1.457	-.0005	.0087	-.1.237	.0544	.0390	.0779	.2041	.1302	.271			
5	-	-.0042	-	-.0042	.0043	.1256	.1736	.451	.1256	.1573	6.052	-	-.0412	-.0800	-.0512	-.0224	-.313				
6																					
ANTI-SYMMETRICAL MOTION																					
ϕ'																					
1	58.46	86.72	-	.994	1.050	-	-.0933	-1.552	-221.0	9.938	14.22	13.21	39.785	65.66	181.72						
2	4.97	3.12	-	.1047	.0777	-	-.0095	-.1587	-.22.25	1.085	.8339	1.402	5.347	9.292	10.172						
3	.266	.1762	-	.0055	.0040	.0243	-.0005	-.0087	-.1.237	.0544	.0390	.0779	.2041	.3302	.574						
4	-	-.206	-	-.0042	.0043	.1256	.1573	6.052	-	-.0412	-.0800	-.0512	-.0224	-.256							

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Prepared	Approved	Page
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卷之三

Wt.	35,000 ft.	q	- 120
	- 11,500 lbs.	q	- 570 ft./sec.
	- 105,000 lbs.	a	.175 ft.
		CG&q	.280

Alt. 47
W 29
W 84

1

1

1

10

PREPARED
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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION RUNS 1423, 18239, 240																				
SYMMETRICAL MOTION																				
ω .. ω . ω .. ψ .. ψ . θ .. θ . α .. α . β .. β . κ .. κ . κ .. κ . β .. β . β .. β . β .. β .																				
.0331	.0214	-	.0110	.0091	-	.0203	.1237	.12.217	.0010	.0173	.2.928	.10.88	.0834	.1888	.4411	.6934	.7.7822			
.0203	.0286	-	.03714	.0353	-	.7.612	.5.744	.18.64	.2549	.3736	.9.38	.2706	-.3479	-.686	.1.490	.2.294	.5.9392			
.0544	.0128	-	.1047	.0777	-	.1.1653	-.1754	.24.36	-.0095	-.1587	.22.25	.1.085	.8339	.1402	.5.267	.9.292	.8.5012			
.0020	.0026	-	.0055	.0040	.0243	-.0101	-.0096	.1.457	-.0005	-.0087	.1.237	.0564	.0390	.0779	.2041	.3302	.3771			
	-.0022	-		-.0042	.0043	.1256	.1736	.461	.1256	.1573	.6.052	-	-.012	-.0800	-.0512	-.0224	.313X			
ANTI-SYMMETRICAL MOTION																				
ϕ .. ϕ . ϕ .. ψ .. ψ . θ .. θ . α .. α . β .. β . β .. β . β .. β . β . β .. β . β . β .. β . β .																				
60.228	86.72	-	.994	1.050	-	-.0923	-.1.552	.221.0	9.938	14.29	13.31	39.79	65.66	181.7X						
4.97	3.12	-	.10.7	.0777	-	-.0095	-.1587	.22.25	1.085	.8339	1.402	5.347	9.290	10.37X						
.266	.1762	-	.0055	.0010	.0243	-.0095	-.0087	1.237	.0564	.0390	.0779	.2041	.3302	.574X						
	.206	-			.0012	.0013	.1256	.1.573	.6.052	-	-.0412	-.0800	.0512	-.0224	-.256X					

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Alt. 35,000 ft. V = 570 ft/sec.
W₄ 11,500# a = .175 ft.
W₂₉ 120,000# CCS₄ = .280
W₂₀ 120

101-A
EDR-C905-104

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
TABLE II-D COEFFICIENTS OF EQUATIONS OF MOTION NOS # 241, 242, 243																					
SYMMETRICAL MOTION																					
ω_{ij} ω_j ω_i α_{ij} α_i α_j θ_{ij} θ_i θ_j β_{ij} β_i β_j C_{ij} C_i C_j G_{ij} G_i G_j K_{ij} K_i K_j $F.F.$																					
Eq. 1	.02702	.0214	-	.0110	.0091	-	.0203	.1237	.12.217	.0010	.0173	.2.998	.1088	.0634	.1888	.4411	.6934	.4411	.6934	.4411	.6934
2	.0203	-.0316	-	-.0374	-.0353	-	-.0374	-.0353	-.0374	-.0353	-.0374	-.0353	-.0374	-.0374	-.0374	-.0374	-.0374	-.0374	-.0374	-.0374	-.0374
3	.0264	.0125	-	.1047	.0777	-	-.1853	-.1754	-.1754	-.1754	-.1754	-.1754	-.1754	-.1754	-.1754	-.1754	-.1754	-.1754	-.1754	-.1754	
4	.0030	.0026	-	.0055	.0040	.00243	-.0101	-.0096	-.0096	-.01457	-.0095	-.0137	-.0137	.0544	.0390	.0779	.2041	.3022	.3022	.3022	
5	-	-.0022	-	-	-.0042	.0043	.1256	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	
ANTI-SYMMETRICAL MOTION																					
α_{ij} α_i α_j β_{ij} β_i β_j γ_{ij} γ_i γ_j ω_{ij} ω_i ω_j θ_{ij} θ_i θ_j C_{ij} C_i C_j G_{ij} G_i G_j K_{ij} K_i K_j $F.F.$																					
Eq. 1	62.05	36.12	-	.994	1.050	-	-.0933	-.1552	-.221.0	9.933	11.29	13.91	39.785	131.71	65.66	131.71	65.66	131.71	65.66	131.71	
2	4.97	3.12	-	.1047	.0777	-	-.0095	-.1587	-.22.25	1.015	.2339	1.402	5.367	9.292	10.17X						
3	.266	.1762	-	.0055	.0040	.0243	-.0005	-.0087	-.1.37	.0544	.0390	.0779	.2041	.3302	.574 X						
4	-	-.206	-	-	-.0042	.0043	.1256	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	.1736	

PREPARED
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REVISION

Alt. S.L. V 344 FT./SEC.
W24 -13,000 F 0 -.175
W29 -105,000 F 0 .233
q 140 0684

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TABLE II-D
COEFFICIENTS OF EQUATIONS OF MOTION
RUNS # 47, 248, 249

SYMMETRIC MOTION												ANTI-SYMMETRIC MOTION											
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21		
Eq. 1	ω_1	ω_2	ω_3	ω_4	ω_5	ω_6	ω_7	ω_8	ω_9	ω_{10}	ω_{11}	ω_{12}	ω_{13}	ω_{14}	ω_{15}	ω_{16}	ω_{17}	ω_{18}	ω_{19}	ω_{20}	ω_{21}	ω	
Eq. 2	.02906	.03552	-	.01066	.01512	-	.01753	-	.02550	.12.217	.001010	.2022812	2.998	.1056	.1382	.1888	.4411	.6924	.85823				
Eq. 3	-	-.01763	.06401	-	.02257	.05835	-	.05230	9.5203	18.64	.2159	.6192	9.38	.2226	-.5766	-.686	-.14620	-.2224	6.49212				
Eq. 4	.05281	.07096	-	.1021	.1287	-	.1613	-	.2907	24.36	.009245	.2651	22.25	1.0548	1.2819	1.402	.5267	.9292	.95522				
Eq. 5	.002886	.004217	-	.005332	.006596	.007079	-.008817	.01587	.1457	.0005051	.01436	1.237	.05280	.06471	.0779	.2041	.3302	.4192					
Eq. 6	-	.005001	-	-	.009065	.003638	.1095	.2878	.9380	.1095	.2607	5.661	-	-.08922	-.1051	-.1202	-.1353	-.2096					

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X X

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114	- \$1.000*	V - .410
164	- 13,000*	A - .175
129	- 105,000*	C.G. - .233
0	200	C.G. - .233

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

TABLE II - EQUATIONS OF MOTION.
RATIO = 250, FOL 252

SYMMETRIC MOTION

	ω_1	ω_2	ω_3	ω_4	ω_5	ω_6	ω_7	ω_8	ω_9	ω_{10}	ω_{11}	ω_{12}	ω_{13}	ω_{14}	ω_{15}	ω_{16}	ω_{17}	ω_{18}	ω_{19}	ω_{20}	ω_{21}
Eq. 1	.02034	.02980	-	.007464	.012688	-	.01234	.01234	.01234	.01234	.01234	.01234	.01234	.01234	.01234	.01234	.01234	.01234	.01234	.01234	
2	-.01234	-.05371	-	-.02280	.01612	-	-.02280	-.02280	-.02280	-.02280	-.02280	-.02280	-.02280	-.02280	-.02280	-.02280	-.02280	-.02280	-.02280	-.02280	
3	.03697	.05954	-	.07248	.1080	-	.07248	.07248	.07248	.07248	.07248	.07248	.07248	.07248	.07248	.07248	.07248	.07248	.07248	.07248	
4	.00202	.003562	-	.003733	.005526	-	.01155	.006172	-.01322	-.01322	-.01322	-.01322	-.01322	-.01322	-.01322	-.01322	-.01322	-.01322	-.01322	-.01322	
5	-	-.004196	-	-	-.007506	-	.00247	.07668	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	

ASYMMETRIC MOTION

	ω_1	ω_2	ω_3	ω_4	ω_5	ω_6	ω_7	ω_8	ω_9	ω_{10}	ω_{11}	ω_{12}	ω_{13}	ω_{14}	ω_{15}	ω_{16}	ω_{17}	ω_{18}	ω_{19}	ω_{20}	ω_{21}
Eq. 1	39.9574	120.5639	-	6759	1.6400	-	.065336	-.21565	-.221.0	6.7570	19.754	13.910	39.75	65.660	113.2130	F.F.					
2	3.3315	4.3390	-	.07152	.1080	-	.00668	-.2207	-.22.25	.71.54	1.1595	1.402	5.247	9.292	8.01071						
3	1.810	.2451	-	.003733	.005526	.01155	.0003535	-.01205	- 1.237	.03696	.02429	.0719	.2041	.3202	.45244						
4	-	.3647	-	-	-.007506	-.00247	.07668	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	-.2424	

CONFIDENTIAL

PREPARED
CHECKED
APRIL 1961

Altitude = 20,000 ft. V = 354 ft/sec.
Eq. 1 184 13,000 lbs. a = .175 ft.
Eq. 2 129 105,000 lbs. CG84 = .233
q 80

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1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
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TABLE II - D
COEFFICIENTS OF EQUATIONS OF MOTION
RUNS # 253, 254, 255

SYMMETRIC MOTION

	ω_1	ω_2	ω_3	ω_4	ω_5	ω_6	ω_7	ω_8	ω_9	ω_{10}	ω_{11}	ω_{12}	ω_{13}	ω_{14}	ω_{15}	ω_{16}	ω_{17}	ω_{18}	ω_{19}	ω_{20}
Eq. 1	.0509	.0346	-	.0186	.01469	-	.03086	.01992	.12.237	.001767	.02990	.2.998	.18.8	.13.2				.10.362		
2	-	.0509	-.06216	-	-.05669	-.05689	-	.11.12	.9.251	.18.64	.3779	.6017	.9.38	-.5616	-.5604				.7.716	
3	.0924	.06890	-	.1787	.1252	-	-.2823	-.2825	.24.36	.01617	-.2556	-.22.25	.1.865	.1.362				.11.316		
4	.0051	.00447	-	.0093	.006410	.03638	-.01543	-.01542	.1.457	.0008838	-.01395	-.1.237	.09242	.06288				.0559		
5	-	-.00449	-	-	.008806	.006366	.0206	.2797	.9381	.1916	.2534	.9.223	-	-.08673				-.11.143		

ANTI-SYMMETRIC MOTION

	α	β	γ	δ	ϵ	ζ	η	θ	β'	β									
Eq. 1	99.90	139.6	-	1.639	1.691	-	.1584	-.2.500	-.221.0	16.92	23.13								
2	8.456	5.025	-	.1787	.1252	-	.01617	-.2556	-.22.25	1.865	1.362								
3	.6526	.2839	-	.009333	.006410	.03638	.0008838	-.01395	-.1.237	.09242	.06288								
4	-	.4226	-	-	.008806	.006366	.0206	.2534	.9.223	-	-.08684								

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Alt. = 20,000 ft. V = 434 ft/sec
W₄ = 13,000 lb. a = 175 ft.
W₉ = 105,000 lb. cgs₄ = .280
q = 120

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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF EQUATIONS OF MOTION																					
RUNS # 257, 258																					
	ω	ω'	ω''	θ'	θ''	θ'''	φ'	φ''	φ'''	α'	α''	α'''	β'	β''	β'''	γ'	γ''	γ'''	δ'	δ''	
B ₁	.0339	.0282	.0124	.00198	.00057	-.1625	-12.217	-.001178	.02276	-2.298	.1232	.1295	.1388	.1411	.1424	.1434	.1441	.1447	.1454	.1461	
2	-.0206	-.0507	-.0579	-.06640	7.610	7.546	18.64	.2519	.4908	9.38	-.3764	-.4571	-.6366	-.4571	-.6366	-.1490	-.2234	6.224			
3	.0616	.0562	.1131	.1321	-.13882	-.2304	-.24.36	.01078	-.2035	-.22.25	1.4.43	1.095	1.02	5.347	9.232						
4	.0034	.0034	.0062	.00528	.02425	-.01258	-.01.57	.005892	-.01188	-.01.37	.06161	.05129	.0779	.0244	.0302	.04045					
5					-.007183	-.004244	.1277	.2281	.9381	.1277	.2067	6.4525		-.07074	-.1051	-.12022	-.1353	-.3379			
SYMMETRIC MOTION																					
B ₁	ω	ω'	ω''	θ'	θ''	θ'''	φ'	φ''	φ'''	α'	α''	α'''	β'	β''	β'''	γ'	γ''	γ'''	δ'	δ''	
2	64.60	113.9	1.16	1.377	.1036	-.039	-22.0	11.28	18.78	13.21	39.79	65.66	183.0								
3	5.637	4.099	.1191	.1021	.01078	-.2085	-.22.25	1.243	1.095	1.02	5.347	9.232	10.24								
4	.3017	.2316	.006222	.005228	.005228	-.01138	-.1.237	.01161	.05129	.0779	.2041	.3302	.5783								
					-.007183	-.004244	.1277	.2067	6.4525	-.07083	-.1051	-.1202	-.1353	-.2578							
ASYMMETRIC MOTION																					
B ₁	ψ	ϑ	ϑ'	ϑ''	ϑ'''	α'	α''	α'''	β'	β''	β'''	γ'	γ''	γ'''	δ'	δ''	δ'''	β'	β''		
2																					
3																					
4																					

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Alt. = 20,000 ft. V = 50 ft/sec
W84 = 13,300 # a = 1.175 ft.
W29 = 105,300 # $cg\delta A$ = .280
 q = 160

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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21

COEFFICIENTS TABLE III-D
OF EQUATIONS OF MOTION
DUNS 352-260261

	ω'	ω	ω	β'	β	β	α'	α	α	γ'	γ	γ	δ'	δ	δ	β'	β	β	β'	β	
Eq. 1	.0234	.02443		.01098	.01093		-.01543	-.01408		-12.217	.00835		-.01972	-2.998		.09485					
2	-.01545	.01392		-.04019	-.0284		5.7075	6.537		18.64	.1387		.4252	9.38		-.3960					
3	.0462	.04868		.0834	.0893		-.1412	-.1996		-24.36	.008085		-.1806	-22.25		.9223	.9485				
4	.00255	.002265		.004229	.01819		.00772	-.01090		-1.457	.0004119		-.008358	-1.237		.04621	.04463				
5	-.00327			-.008222	-.03183		.09578	.1976		.9381	.09573		.1791	5.067		-.06128					

ANTI-SYMMETRIC MOTION

	ψ'	ψ	ϕ'	ϕ	γ'	γ	α'	α	β'	β	β	β	γ'	γ	γ	α'	α	β'	β	β	β'
Eq. 1	49.95	98.67		.8445	1.195		.0792	-.1766		-221.0	8.46		16.27								
2	4.228	3.551		.08933	.0884		.008085	-.1806		-22.25	.3233		.9485								
3	.2263	.2006		.004667	.004229		.01819	.0004119		-.009858	-.1237		.04621	.04443							
4		-.2384		-.008222	-.03183		.09578	.1791		5.067			-.06136								

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PREPARED _____
 CHECKED _____
 REVISED _____

Alt. ■ 35,000 ft. V ■ 465
 W84 ■ 13,300 ft. A ■ 175 ft.
 W29 ■ 105,000 lbs. Cg ■ .280
 q ■ 80

REF ID: A65f 108
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 REVISERED

TABLE I
 COEFFICIENTS FOR EQUATIONS OF MOTION
 BASIS ■ 262,263,264

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
SYMMETRIC MOTION																					
α																					
E_1	.05035	.02628	.01866	.01118	-.03086	-.1516	-.12.219	-.001767	-.02125	-.2.988	.1848	.1022	.1888	.4411	.6934	-.9.554					
E_2	-.0086	-.04735	.06702	-.04331	.11.42	7.043	18.64	.3777	.6580	.9.28	-.5646	-.4266	-.6860	-.1.490	-.2.294	7.283					
E_3	.09241	.05249	.1787	.09257	-.2.823	-.2550	-.26.36	.01617	-.1.346	-.22.25	1.865	1.022	1.432	5.347	9.232	10.42					
E_4	.005050	-.003442	.003337	.004880	.03638	-.02543	-.01175	-.1.457	.0008838	-.01062	-.1.237	.01242	.06787	.0779	.2.041	.33102	.45449				
E_5	.003700				-.005125	.006366	.1916	.2129	.4610	.1916	.1.229	.2.223	-.06402	-.1.051	-.1.2022	-.1.353	-.3834				
ANTI-SYMMETRIC MOTION																					
α																					
E_1	82.30	36.06	1.352	1.151	.1584	-.1.704	-.221.0	13.54	15.67	13.91	39.79	65.66	129.2								
E_2	6.764	3.421	.2630	.08319	.1617	-.1740	-.22.25	1.432	.3240	1.422	5.347	9.492	11.14								
E_3	.3620	.1.332	.007466	.002910	.0008338	-.009437	-.1.237	.0739	.04281	.0779	.2041	.33102	.6234								
E_4	-.3516				-.006704	.005092	.1916	.1725	.9.223	-.06610	-.1.51	-.1.202	-.1.353	-.2.805							

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Alt.	35,000 ft.	V	520 ft./sec
■ B2	13,000 ft.	a	.175
■ B29	105,000 ft.	g	.233
q	100		

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REVISED

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W.D.C.

RUNS # 265 266 267

PREPARED _____
 CHECKED _____
 REVIEWED _____
 DATE _____
 BY DR-C90504

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Alt. = 35,000 ft. V = 570 ft/sec
 W84 = 13,700 # a = -175
 W29 = 105,000 # c_g = .233
 q = 120

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	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21
COEFFICIENTS OF MOTION.																					
TABLE II-D RUNS # 268, 269, 270																					
	w	w'	w''	w'''	w'''	w''''	w'''''	w'''''	w''''''	w'''''''	w'''''''	w''''''''	w'''''''''	w''''''''''	w'''''''''''	w''''''''''''	w'''''''''''''	w'''''''''''''''	w''''''''''''''''	w''''''''''''''''''	w'''''''''''''''''''
	Φ	ψ	θ	γ	β	α	θ'	θ''	θ'''	θ''''	θ'''''	θ'''''	θ''''''	θ'''''''	θ''''''''	θ''''''''''	θ'''''''''''	θ'''''''''''''	θ''''''''''''''	θ''''''''''''''''	θ'''''''''''''''''
1	.03320	.002144	.01244	.002121	-.02057	.02237	-12.217	.00178	.01734	.2.998	.2232	.08337	-.7.74								
2	-.2407	-.0.865	-.2.801	-.0.533	7.613	5.746	13.64	.2512	.2736	2.38	.3754	-.3480	5.260								
3	.06161	.04282	.1191	.07772	-.1882	-.1754	-.24.36	.01078	-.1588	-22.25	1.243	.8337	8.501								
4	.00367	.002363	.06225	.003781	.06425	-.01329	-.009586	-.1.457	.0.005892	-.008664	-.1.237	.06161	.03905	.3711							
5	.003018				.04181	.004264	.1277	.1737		.12.77	.1.574	.05326	-.31228								
ANTI-SYMMETRICAL MOTION																					
	Φ	ψ	θ	γ	β	α	θ'	θ''	θ'''	θ''''	θ'''''	θ'''''	θ''''''	θ'''''''	θ''''''''	θ''''''''''	θ'''''''''''	θ'''''''''''''	θ''''''''''''''	θ''''''''''''''''	θ'''''''''''''''''
1	.54.67	17.35	.2013	.93.0	.09533	.56950	.01240	.0095822	-.0.07748	-.1.237	.0.027	.034.92	1.28.5	1.083							
2	4.539	2.721	.0776	.074777	.003552	.01240	.0095822	-.0.07748	-.1.237	.0.027	.034.92	1.28.5	1.083	.5135							
					.005469	.003395	.02777	.0.007	6.45		-.0.5326	-.2.288									

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TABLE III-A

MAXIMUM AMPLITUDES OF OSCILLATION

SYMMETRICAL MOTION

(CONFIDENTIAL)

TABLE III-A

SYMMETRICAL MOTION

MAX. AMPLITUDES OF OSCILLATIONS

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RUN	Θ (RAD.)	β (RAD.)	y (FT)	α (RAD.)
1	+ .0125	- .245	± .110	+ .0040
2	+ .0119	- .080	- .220	+ .0040
3	+ .0112	- .046	- .250	+ .0040
4	+ .0125	- .250	+ .1025	+ .00375
5	+ .0114	- .0735	- .2175	+ .00375
6	+ .01125	- .0440	- .245	+ .00375
7	+ .0125	- .240	+ .1025	+ .00352
8	+ .01125	- .070	- .205	+ .00352
9	+ .01075	- .0405	- .2275	+ .00352
10	+ .01273	- .278	- .2820	- .0048
11	+ .0119	- .080	- .3700	+ .0048
12	+ .0114	- .0450	- .4100	+ .0049
13	+ .0125	- .278	- .252	- .0049
14	+ .0119	- .0747	- .352	+ .0045
15	+ .0113	- .0430	- .400	+ .0046
16	+ .0124	- .270	- .180	- .0042
17	+ .0113	- .0705	- .350	+ .0043
18	+ .0113	- .0400	- .387	+ .0044
19	+ .0125	- .298	- .330	- .0065
20	+ .0115	- .0775	- .492	+ .0051
21	+ .0113	- .0450	- .0570	+ .0055
22	+ .0125	- .2320	- .2750	- .0060
23	+ .0113	- .0750	- .490	+ .0050
24	+ .0113	- .0435	- .0550	+ .0052
25	+ .0123	- .2920	- .310	- .0065
26	+ .0113	- .0750	- .450	+ .0048
27	+ .0109	- .0435	- .530	+ .0050
28	+ .0128	- .248	+ .1026	+ .0038

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TABLE III-A (CONT'D)

SYMMETRICAL MOTION

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RUN	θ (RAD.)	β (RAD.)	y (FT.)	α (RAD.)
29	+ .0119	-.0750	-.220	+ .0038
30	+ .0113	-.0450	-.248	+ .0038
31	+ .0125	-.2450	.1025	+ .0035
32	+ .0114	-.0710	-.2125	+ .0035
33	+ .0113	-.0440	-.2200	+ .0038
34	+ .0125	-.2400	.1025	+ .0035
35	+ .0113	-.0685	-.2000	+ .0035
36	+ .0112	-.0410	-.2050	+ .0035
37	+ .0126	-.2800	-.2350	-.0046
38	+ .01189	-.078	-.372	+ .0045
39	+ .01189	-.046	-.390	+ .0048
40	+ .0125	-.284	-.1925	-.0044
41	+ .0113	-.0755	-.3525	+ .0044
42	+ .0113	-.0425	-.4000	+ .0044
43	+ .0125	-.2820	-.1750	-.0044
44	+ .0113	-.0725	-.3280	+ .0041
45	+ .0113	-.0410	-.3750	+ .0043
46	+ .0125	-.3000	-.3050	-.0065
47	+ .0113	-.0300	-.4900	+ .0050
48	+ .0113	-.045	-.5500	+ .0053
49	+ .0125	-.2980	-.2550	-.0063
50	+ .0113	-.0748	-.4800	+ .0045
51	+ .0108	-.0450	-.550	+ .0043
52	+ .0124	-.2940	-.255	-.0063
53	+ .0113	-.0705	-.450	+ .0045
54	+ .0106	-.0400	-.530	+ .0046
55	+ .0131	-.2520	-.1075	+ .00367
56	+ .0119	-.0795	-.2360	+ .0038

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TABLE III-A (CONT'D)
SYMMETRICAL MOTION

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RUN	Θ (RAD.)	β (RAD.)	y (FT.)	α (RAD.)
57	+ .0114	-.0450	-.2500	+ .0038
58	+ .0127	-.2500	-.1250	+ .0035
59	+ .0113	-.0675	-.205	+ .0035
60	+ .0113	-.0400	-.225	+ .0037
61	+ .0125	-.2450	-.1175	+ .0034
62	+ .0113	-.0655	-.2000	+ .0035
63	+ .0106	-.0400	-.2250	+ .0035
64	+ .0130	-.2300	-.2000	- .0045
65	+ .0124	-.079	-.3500	+ .0044
66	+ .0119	-.0470	-.4050	+ .0045
67	+ .0125	-.2300	-.1525	- .0041
68	+ .0114	-.0740	-.3500	+ .0041
69	+ .0113	-.0400	-.3875	+ .0043
70	+ .0125	-.2700	-.1650	- .0043
71	+ .0113	-.0655	-.3620	+ .0039
72	+ .0111	-.0350	-.3745	+ .0040
73	+ .0125	-.3000	-.3000	- .0066
74	+ .0115	-.0750	-.4750	+ .0050
75	+ .0111	-.045	-.5550	+ .0050
76	+ .0125	-.3000	-.250	- .0062
77	+ .0111	-.075	-.485	+ .0045
78	+ .0111	-.0425	-.550	+ .0046
79	+ .0124	-.290	-.225	- .0060
80	+ .0110	-.0695	-.450	+ .0043
81	+ .0106	-.0400	-.500	+ .0045
82	+ .0137	-.2900	-.115	+ .0036
83	+ .0125	-.085	-.2380	+ .0037
84	+ .0125	-.0500	-.2750	+ .0038

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RUN	θ (RAD)	β (RAD)	y (FT.)	α (RAD)
85	+ .0138	-.3000	±.1000	+ .0035
86	+ .0125	-.0805	-.2370	+ .0035
87	+ .0119	-.0450	-.2600	+ .0035
88	+ .0138	-.2940	±.1000	+ .0033
89	+ .0124	-.0770	-.2250	+ .0033
90	+ .0113	-.0425	-.250	+ .0034
91	+ .0138	-.3000	-.1825	+ .0041
92	+ .0124	-.0875	-.3500	+ .0043
93	+ .0120	-.0495	-.3950	+ .0043
94	+ .0136	-.3000	-.1675	+ .0040
95	+ .0123	-.0795	-.3250	+ .0040
96	+ .0113	-.045	-.3750	+ .0040
97	+ .0125	-.3000	-.1500	- .0040
98	+ .0116	-.0750	-.3250	+ .0038
99	+ .0113	-.0425	-.3500	+ .0040
100	+ .0136	-.3200	-.2500	- .0054
101	+ .0125	-.0850	-.4250	+ .0046
102	+ .0119	-.0475	-.5000	+ .0048
103	+ .0130	-.3200	-.2280	- .0053
104	+ .0119	-.0300	-.4150	+ .0043
105	+ .0113	-.0450	-.4350	+ .0045
106	+ .0128	-.3200	-.2250	- .0053
107	+ .0121	-.0750	-.4150	+ .0041
108	+ .0113	-.0405	-.4600	+ .0043
109	+ .0139	-.2980	-.1025	+ .0035
110	+ .0125	-.0850	-.2480	+ .0035
111	+ .0125	-.0475	-.2750	+ .0037
112	+ .0138	-.2900	-.1025	+ .0034

(CONFIDENTIAL)

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RUN	θ (RAD)	β (RAD.)	y(FT)	α (RAD)
113	+ .0125	-.0800	-.2350	+ .0034
114	+ .0116	-.04500	-.252	+ .0035
115	+ .0138	-.2900	+.1000	+ .0031
116	+ .0119	-.07500	-.1125	+ .0032
117	+ .0113	-.043	-.250	+ .0033
118	+ .0138	-.3000	-.1875	- .0041
119	+ .0125	-.0900	-.3620	+ .0023
120	+ .0119	-.0495	-.375	+ .0025
121	+ .0135	-.3100	-.165	- .0040
122	+ .0119	-.0800	-.3400	+ .0021
123	+ .0113	-.0450	-.3750	+ .0022
124	+ .0129	-.3000	-.1525	- .0039
125	+ .0118	-.0745	-.3250	+ .0036
126	+ .0113	-.0400	-.3500	+ .0039
127	+ .0134	-.3200	-.225	- .0053
128	+ .0125	-.0825	-.4250	+ .0044
129	+ .0119	-.04500	-.4975	+ .0045
130	+ .0126	-.3200	-.2125	- .0054
131	+ .0119	-.0770	-.4220	+ .0041
132	+ .0114	-.0435	-.4750	+ .0043
133	+ .0126	-.3300	-.2250	- .0054
134	+ .0119	-.0750	-.3750	+ .0040
135	+ .0113	-.0400	-.450	+ .0042
136	+ .0140	-.3000	-.1250	+ .0034
137	+ .0126	-.0805	-.2400	+ .0035
138	+ .0125	-.0450	-.2500	+ .0036
139	+ .0138	-.2820	+.1000	+ .0033
140	+ .0125	-.0755	-.2325	+ .0033

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TABLE III-A (CONT'D) CONFIDENTIAL
SYMMETRICAL MOTION117
EDR-C905-104

RUN	θ (RAD)	β (RAD)	y (FT.)	α (RAD)
141	+ .0119	-.0425	-.2500	+ .0034
142	+ .0138	-.2800	+.1000	+ .0031
143	+ .0113	-.0725	-.2250	+ .0031
144	+ .0111	-.0400	-.2320	+ .0033
145	+ .0138	-.3000	-.1525	- .0043
146	+ .0125	-.0300	-.350	+ .0040
147	+ .0119	-.045	-.387	+ .0040
148	+ .0136	-.3000	-.150	- .0041
149	+ .0124	-.0750	-.328	+ .0040
150	+ .0113	-.0400	-.367	+ .0039
151	+ .0131	-.3000	-.150	- .0040
152	+ .0115	-.0715	-.325	+ .0035
153	+ .0113	-.0376	-.3500	+ .0038
154	+ .0138	-.3300	-.2150	- .0054
155	+ .0125	-.0300	-.427	+ .0043
156	+ .0113	-.0450	-.495	+ .0044
157	+ .0136	-.3100	-.1775	- .0053
158	+ .0123	-.0750	-.405	+ .0040
159	+ .0113	-.0425	-.463	+ .0043
160	+ .0131	-.3100	-.1750	- .0051
161	+ .0118	-.0705	-.4000	+ .0039
162	+ .0113	-.0400	-.4400	+ .0040
163	+ .01440	-.3260	-.1275	+ .0035
164	+ .0131	-.0895	-.2650	+ .0036
165	+ .0125	-.0500	-.2900	+ .0036
166	+ .0138	-.3200	-.1250	+ .0033
167	+ .0125	-.0855	-.2500	+ .0033
168	+ .0124	-.0455	-.2770	+ .0035

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TABLE III-A (CONT'D) [CONFIDENTIAL]
SYMMETRICAL MOTION118
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RUN	θ (RAD.)	β (RAD.)	y (FT.)	α (RAD.)
169	+ .0138	- .3100	- .1125	+ .0033
170	+ .0125	- .0815	- .2500	+ .0032
171	+ .0113	- .0445	- .2650	+ .0033
172	+ .0144	- .3300	- .1525	- .0040
173	+ .0130	+ .0900	- .3000	+ .0039
174	+ .0125	- .0500	- .3500	+ .0040
175	+ .0138	- .326	- .1375	- .0039
176	+ .0125	- .0850	- .3050	+ .0036
177	+ .0119	- .0455	- .3300	+ .0037
178	+ .0138	- .3200	- .1275	- .0037
179	+ .0125	- .0800	- .2980	+ .0035
180	+ .0113	- .0440	- .3250	+ .0035
181	+ .0150	- .3600	- .1750	- .0050
182	+ .0136	+ .1000	- .3750	+ .0044
183	+ .0125	+ .0600	+ .4000	+ .0045
184	+ .0148	- .344	- .175	- .0048
185	+ .0131	- .0890	- .352	+ .0041
186	+ .0125	+ .0500	- .4070	+ .0042
187	+ .0138	- .3500	- .1525	- .0048
188	+ .0125	- .0875	+ .332	+ .0039
189	+ .0119	- .0460	- .3750	+ .0040
190	+ .0144	- .3200	- .125	+ .0034
191	+ .0131	- .0900	- .258	+ .0035
192	+ .0125	- .0500	- .2880	+ .0035
193	+ .0138	- .3200	- .125	+ .0033
194	+ .0125	- .0845	- .2500	+ .0033
195	+ .0119	- .0450	- .2750	+ .0033
196	+ .0138	- .3200	- .125	+ .0030

CONFIDENTIAL

[CONFIDENTIAL]

TABLE III-A (CONT'D)
SYMMETRICAL MOTION

CONFIDENTIAL

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EDR-C905-104

RUN	Θ (RAD)	β (RAD)	y(FT.)	α (RAD)
197	+ .0124	-.0800	-.245	+ .0031
198	+ .0113	-.0430	-.260	+ .0030
199	+ .0144	-.3400	-.130	- .0040
200	+ .0128	-.0875	-.297	+ .0038
201	+ .0125	-.0495	-.350	+ .0038
202	+ .0140	-.334	-.125	- .0039
203	+ .0125	-.0845	-.300	+ .0035
204	+ .0119	-.0450	-.325	+ .0035
205	+ .0138	-.3300	-.125	- .0038
206	+ .0125	-.081	-.3000	+ .0033
207	+ .0113	-.042	-.312	+ .0035
208	+ .0141	-.3600	-.175	- .0050
209	+ .0129	-.0905	-.352	+ .0043
210	+ .0125	+ .0545	-.415	+ .0043
211	+ .0138	-.3500	-.175	- .0049
212	+ .0125	+ .0875	-.338	+ .0040
213	+ .0119	-.0495	-.4000	+ .0040
214	+ .0138	-.3400	-.1500	- .0045
215	+ .0125	-.0805	-.3250	+ .0037
216	+ .0115	-.0450	-.3750	+ .0038
217	+ .0150	-.3300	-.1125	+ .0033
218	+ .0131	-.0880	-.2630	+ .0035
219	+ .0125	-.0475	-.2730	+ .0035
220	+ .0139	-.3200	-.1023	- .0033
221	+ .0125	-.0825	-.2500	+ .0033
222	+ .0119	-.0450	-.2650	+ .0033
223	+ .0138	-.3180	-.1025	+ .0030
224	+ .0121	-.0825	-.2480	+ .0030

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TABLE III-A (CONT'D)
SYMMETRICAL MOTION

CONFIDENTIAL

120
EDR-C905-104

RUN	θ (RAD.)	β (RAD.)	y (FT.)	α (RAD.)
225	+ .0113	-.0405	-.2500	+ .0030
226	+ .0149	-.3400	-.1250	-.0042
227	+ .0128	-.0855	-.3000	+ .0037
228	+ .0125	-.0455	-.3400	+ .0038
229	+ .0138	-.3400	-.1500	-.0039
230	+ .0125	-.0850	-.3000	+ .0035
231	+ .0118	-.0440	-.323	+ .0035
232	+ .0137	-.3300	+ .1275	-.0036
233	+ .0119	-.0755	-.2800	+ .0033
234	+ .0113	-.0400	-.3000	+ .0033
235	+ .0144	-.3600	-.1500	-.0050
236	+ .0128	-.0890	-.3750	+ .0040
237	+ .0125	-.5000	-.4100	+ .0041
238	+ .0138	-.3540	-.1375	-.0050
239	+ .0125	-.0850	-.3520	+ .0038
240	+ .0119	-.0450	-.3770	+ .0039
241	+ .0138	-.3400	+ .1250	-.0048
242	+ .0124	-.0795	-.3250	+ .0037
243	+ .0114	-.0450	-.3750	+ .0033
244	+ .0125	-.2500	+ .1150	+ .0033
245	+ .0119	-.0725	-.2125	+ .0032
246	+ .0113	-.0435	-.2450	+ .0032
247	+ .0125	-.2780	-.2750	-.0048
248	+ .0114	-.0735	-.3720	+ .0037
249	+ .0113	-.0405	-.3875	+ .0037
250	+ .0125	-.2800	-.3745	-.0066
251	+ .0113	-.0750	-.4900	+ .0039
252	+ .0113	-.0400	-.563	+ .0040

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TABLE III-A (CONCLUDED)
SYMMETRICAL MOTION

~~CONFIDENTIAL~~

RUN	θ (RAD.)	β (RAD.)	y (FT.)	α (RAD.)
253	+ .0131	-.2800	+.1125	+ .0032
254	+ .0119	-.0775	-.2275	+ .0031
255	+ .0113	-.0450	-.2620	+ .0030
256	+ .0127	-.3000	-.2300	- .0048
257	+ .0124	-.0750	-.3250	+ .0035
258	+ .0113	-.0405	-.3750	+ .0035
259	+ .0125	-.3100	-.3245	- .0063
260	+ .0123	-.0875	-.4370	+ .0038
261	+ .0119	-.0455	-.4750	+ .0037
262	+ .0138	-.3100	-.1125	- .0033
263	+ .0125	-.0825	-.2480	+ .0030
264	+ .0119	-.0445	-.2750	+ .0030
265	+ .0138	-.3220	-.1750	- .0045
266	+ .0125	-.0950	-.3220	+ .0031
267	+ .0125	+.0500	-.3175	+ .0031
268	+ .0137	-.3400	-.2250	- .0054
269	+ .0125	-.0825	-.3375	+ .0034
270	+ .0124	-.0475	-.4000	+ .0035

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TABLE III-B

MAXIMUM AMPLITUDES OF OSCILLATIONS

ANTI-SYMMETRICAL MOTION

CONFIDENTIAL

TABLE III-B
ANTI-SYMMETRICAL CASE

CONFIDENTIAL

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XDR-C905-104

MAXIMUM AMPLITUDES OF OSCILLATIONS

RUN	ψ (RAD. RAD)	β (RAD)	y (FT.)	α (RAD)
1	-.03	-.1093	-.105	.001125
2	-.03	-.0687	-.095	-.00162
3	-.0285	-.05	-.11	-.00200
4	-.03	-.1125	-.075	-.00125
5	-.0275	-.0655	-.095	-.00175
6	-.0275	-.0500	-.155	-.00200
7	-.0250	-.1095	-.085	-.00125
8	-.0250	-.0625	-.090	-.001625
9	-.0250	-.047	-.145	-.00200
10	-.0275	-.100	-.080	-.001625
11	-.0275	-.050	-.130	-.00200
12	-.0262	-.033	-.200	-.00233
13	-.0325	-.1125	-.090	-.00175
14	-.0300	-.0607	-.160	-.00212
15	-.0300	-.0438	-.125	-.00275
16	-.0287	-.1125	-.095	-.00175
17	-.0287	-.0594	-.150	-.00212
18	-.0287	-.0407	-.240	-.00262
19	-.0288	-.122	-.11	-.00333
20	-.0288	-.050	-.21	-.00325
21	-.0275	-.0313	-.26	-.00350
22	-.0325	-.1375	-.14	-.00375
23	-.0312	-.0563	-.12	-.00362
24	-.0300	-.0344	-.32	-.00387
25	-.030	-.1375	-.15	-.00487
26	-.030	-.0563	-.115	-.00325
27	-.0288	-.0344	-.310	-.00363
28	-.030	-.1125	-.090	-.00125

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TABLE III-B (CONT'D)
ANTI - SYMMETRICAL CASE

CONFIDENTIAL

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EDR-C905-104

RUN	φ (RAD/SEC)	B (RAD)	y (FT)	α (RAD)
29	-.0288	-.0688	-.100	-.00175
30	-.02875	-.050	-.155	-.00200
31	-.0275	-.1095	-.075	-.00125
32	-.0275	-.0625	-.0912	-.00175
33	-.0275	-.0375	-.145	-.001875
34	-.0250	-.1062	-.070	-.00125
35	-.0262	-.0594	-.090	-.00175
36	-.0250	-.0438	-.140	-.001875
37	-.0325	-.122	-.125	-.00200
38	-.0325	-.0625	-.170	-.00237
39	-.0312	-.0408	-.250	-.00275
40	-.0312	-.122	-.1125	-.00200
41	-.030	-.0625	-.100	-.00235
42	-.030	-.0375	-.120	-.00272
43	-.030	-.118	-.100	-.001875
44	-.0294	-.0563	-.160	-.00225
45	-.0275	-.0375	-.115	-.00263
46	-.0325	-.135	-.15	-.00360
47	-.0313	-.0563	-.250	-.00363
48	-.0312	-.0344	-.320	-.00375
49	-.0313	-.1375	-.140	-.00350
50	-.030	-.0563	-.140	-.00350
51	-.0313	-.141	-.140	-.00363
52	-.0313	-.134	-.120	-.0035
53	-.0287	-.0532	-.230	-.0035
54	-.0287	-.0312	-.300	-.00363
55	-.0287	-.1125	-.085	-.001875
56	-.0287	-.0657	-.105	-.001875

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TABLE III-B (CONT'D)
ANTI - SYMMETRICAL CASE

CONFIDENTIAL

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EDR-C905-104

RUN	ψ (RAD/SEC)	β (RAD.)	y (=T.)	α (RAD)
57	-.0275	-.097	-.155	-.00213
58	-.0275	-.1095	-.075	-.001375
59	-.0275	-.0625	-.095	-.001875
60	-.0275	-.0437	-.150	-.00223
61	-.0263	-.1062	-.060	-.0015
62	-.0263	-.0563	-.0901	-.00175
63	-.025	-.0407	-.140	-.0020
64	-.0325	-.118	-.130	-.001875
65	-.0315	-.0625	-.170	-.0025
66	-.030	-.0407	-.140	-.00287
67	-.030	-.1188	-.110	-.0020
68	-.030	-.0594	-.165	-.0025
69	-.02875	-.060	-.230	-.00275
70	-.030	-.1155	-.095	-.001875
71	-.0288	-.0563	-.155	-.0025
72	-.0275	-.0375	-.110	-.00263
73	-.0313	-.1405	-.170	-.00375
74	-.0313	-.0563	-.240	-.00363
75	-.030	-.0344	-.300	-.0035
76	-.030	-.1405	-.150	-.00375
77	-.030	-.0563	-.115	-.0035
78	-.030	-.0312	-.300	-.0035
79	-.030	-.1375	-.130	-.0035
80	-.030	-.050	-.220	-.00337
81	-.0288	-.0312	-.28	-.003375
82	-.035	-.150	-.100	-.001375
83	-.035	-.0845	-.125	-.00275
84	-.035	-.0625	-.195	-.00200

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TABLE III-B (CONT'D.) [CONFIDENTIAL] 126
ANTI - SYMMETRICAL CASE EDR-C905-104

RUN	ψ (RAD/SEC)	β (RAD)	y (FT)	α (RAD)
85	-.035	-.1405	-.100	-.00150
86	-.0337	-.0814	-.120	-.00150
87	-.0325	-.0563	-.185	-.001875
88	-.0325	-.1405	$\pm .080$	$\pm .00125$
89	-.0312	-.075	-.110	-.00150
90	-.0312	-.0563	-.175	-.001875
91	-.040	-.1565	-.120	-.0020
92	-.0375	-.1095	-.160	-.001875
93	-.0363	-.0531	-.260	-.0025
94	-.0375	-.150	-.115	-.0020
95	-.0363	-.075	-.200	-.001875
96	-.0337	-.050	-.240	-.00225
97	-.0350	-.144	$\pm .100$	-.001815
98	-.0350	-.0688	-.140	-.001875
99	-.0325	-.050	-.230	-.00237
100	-.0413	-.1625	-.135	-.00262
101	-.0500	-.075	-.215	-.00237
102	-.0375	-.047	-.310	-.00262
103	-.0370	-.1565	-.130	-.00263
104	-.0375	-.072	-.200	-.00225
105	-.0363	-.0469	-.300	-.00287
106	-.0375	-.150	-.120	-.00237
107	-.0350	-.0788	-.180	-.00212
108	-.0350	-.0438	-.290	-.00275
109	-.0363	-.1405	$\pm .075$	-.001375
110	-.0375	-.0813	-.120	-.001625
111	-.035	-.0594	-.190	-.00200
112	-.035	-.1405	$\pm .070$	$\pm .00125$

CONFIDENTIAL

[CONFIDENTIAL]

TABLE III-B (CONT'D) ANTI-SYMMETRICAL CASE

CONFIDENTIAL EDR-127-C905-104

RUN	γ (RAD/SEC)	β (RAD)	y (FT)	α (RAD)
113	-.035	-.0751	-.115	-.00150
114	-.0325	-.0563	-.175	-.001875
115	-.0377	-.134	-.060	±.0125
116	-.0312	-.0719	-.105	-.00150
117	-.0312	-.050	-.170	-.001875
118	-.0380	-.150	±.100	-.001875
119	-.0375	-.075	-.160	-.0020
120	-.0375	-.050	-.240	-.0025
121	-.0375	-.1435	-.100	-.001875
122	-.0363	-.0687	-.150	-.0020
123	-.0337	-.115	-.230	-.00237
124	-.0363	-.1375	-.075	-.001875
125	-.035	-.0658	-.140	-.00213
126	-.0347	-.0437	-.220	-.00225
127	-.0413	-.1565	-.130	-.00263
128	-.0387	-.072	-.220	-.00237
129	-.0388	-.0464	-.300	-.00287
130	-.0387	-.150	-.115	-.00250
131	-.0375	-.0673	-.200	-.00237
132	-.0363	-.0453	-.280	-.00275
133	-.0363	-.1453	-.1525	-.0025
134	-.0357	-.0625	-.180	-.00231
135	-.0350	-.0407	-.270	-.00269
136	-.0363	-.1375	-.0951	-.001375
137	-.0350	-.1375	-.110	-.001625
138	-.0350	-.0563	-.180	-.00200
139	-.0350	-.1375	±.070	-.001375

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TABLE III-B (CONT'D) CONFIDENTIAL

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DR-C905-104

ANTI - SYMMETRICAL CASE

RUN	ϕ (RAD SEC)	β (RAD)	y (FT.)	α (RAD)
140	-.0337	-.0750	-.110	-.001625
141	-.0337	-.0532	-.170	-.0020
142	-.0337	-.134	-.055	-.001375
143	-.0313	-.0605	-.105	-.00175
144	-.0313	-.0470	-.160	-.0020
145	-.0387	-.1435	-.1075	-.00213
146	-.0363	-.0720	-.155	-.0020
147	-.0363	-.050	-.225	-.0025
148	-.0375	-.1435	-.095	-.0020
149	-.0363	-.0688	-.150	-.0020
150	-.0337	-.0469	-.225	-.0025
151	-.035	-.1345	-.075	-.001875
152	-.0337	-.0625	-.140	-.00213
153	-.0337	-.0407	-.210	-.00237
154	-.0416	-.1575	-.130	-.00275
155	-.0275	-.0688	-.210	-.00250
156	-.0387	-.0438	-.300	-.00294
157	-.0387	-.150	-.120	-.00263
158	-.0375	-.0658	-.200	-.00250
159	-.0363	-.0438	-.280	-.00387
160	-.0375	-.1435	-.105	-.00250
161	-.0350	-.0625	-.190	-.00238
162	-.0350	-.0375	-.270	-.00275
163	-.0425	-.0938	-.120	-.00312
164	-.0400	-.100	-.150	-.001375
165	-.0400	-.0688	-.220	-.001875
166	-.0400	-.175	-.100	-.00175

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TABLE III-B (CONT'D) (CONFIDENTIAL)
ANTI - SYMMETRICAL CASE129
EDR-C905-104

RUN	φ (RAD./SEC)	β (RAD.)	y (FT.)	α (RAD.)
167	-.0375	-.0871	-.140	±.001375
168	-.0375	-.0625	-.210	-.001875
169	-.0375	-.1675	-.100	-.001625
170	-.0350	-.0845	-.130	±.001375
171	-.0350	-.0595	-.200	-.00175
172	-.0450	-.1935	-.135	-.00244
173	-.0425	-.0968	-.170	-.001625
174	-.0400	-.0688	-.260	-.00225
175	-.0412	-.1845	-.120	-.00225
176	-.0400	-.0875	-.160	-.001625
177	-.0375	-.0625	-.240	-.00225
178	-.0375	-.169	-.120	-.00212
179	-.0362	-.0813	-.150	-.001625
180	-.0363	-.0564	-.225	-.00212
181	-.0463	-.200	-.170	-.00269
182	-.0437	-.0985	-.180	-.00175
183	-.0425	-.0653	-.280	-.0025
184	-.0437	-.1875	-.150	-.0025
185	-.0413	-.0877	-.160	±.00313
186	-.0400	-.0610	-.260	-.00225
187	-.0400	-.1785	-.140	-.002375
188	-.0387	-.0876	-.160	-.00175
189	-.0375	-.0563	-.260	-.00243
190	-.04375	-.1815	-.100	-.001875
191	-.0400	-.09375	-.140	±.001375
192	-.0400	-.0658	-.215	-.001875
193	-.0400	-.1685	-.0900	-.00175
194	-.0375	-.140	-.0876	-.001375
195	...			

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TABLE III-B (CONT'D.)
ANTI-SYMMETRICAL CASE

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EDR-C905-104

RUN	ψ (RAD./SEC)	β (RAD.)	y (FT.)	α (RAD.)
195	-.0375	-.0625	-.200	-.001875
196	-.0375	-.1625	-.070	-.001625
197	-.0363	-.0815	-.130	-.00150
198	-.035	-.0564	-.185	-.001935
199	-.045	-.100	-.130	-.00237
200	-.0425	-.0875	-.165	-.00175
201	-.0412	-.0642	-.250	-.00225
202	-.0413	-.175	-.110	-.00213
203	-.0400	-.0845	-.150	±.001565
204	-.0388	-.0563	-.230	-.00213
205	-.0400	-.175	-.0951	-.00200
206	-.0375	-.0783	-.145	-.00175
207	-.0363	-.0532	-.220	-.00215
208	-.0463	-.1935	-.165	-.00387
209	-.0437	-.0970	-.180	-.00175
210	-.0425	-.0658	-.280	-.00250
211	-.0450	-.1875	-.130	-.00250
212	-.0425	-.077	-.165	-.001815
213	-.0400	-.061	-.270	-.00250
214	-.0425	-.1815	-.115	-.002375
215	-.0400	-.0813	-.160	-.001875
216	-.0380	-.086	-.250	-.00237
217	-.0425	-.175	±.1265	-.001875
218	-.0413	-.0923	-.125	-.00150
219	-.0400	-.0658	-.205	-.0020
220	-.0413	-.1625	-.0826	-.001625
221	-.0387	-.0845	-.125	-.00150
222	-.0375	-.0595	-.190	-.001875.

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TABLE III-B (CONT'D.)
ANTI-SYMMETRICAL CASE

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EDR-C905-104

RUN	γ (RAD/SEC)	β (RAD)	τ (FT)	α (RAD)
223	-.0375	-.1565	-.065	-.001565
224	-.0363	-.0782	-.120	-.001565
225	-.0350	-.0532	-.142	-.001875
226	-.0444	-.175	-.0650	-.00206
227	-.0425	-.0876	-.1475	-.00175
228	-.0413	-.0595	-.230	-.00225
229	-.0413	-.1687	-.1475	-.00200
230	-.040	-.0813	-.145	-.00175
231	-.0388	-.0532	-.220	-.00225
232	-.0387	-.1625	-.075	-.00206
233	-.0375	-.0735	-.135	-.00175
234	-.0350	-.050	-.205	-.00225
235	-.0463	-.1935	-.160	-.00225
236	-.0443	-.0939	-.1725	-.001815
237	-.0431	-.0625	-.270	-.00244
238	-.0437	-.1845	-.135	-.00231
239	-.0418	-.0845	-.160	-.001875
240	-.0406	-.0595	-.250	-.00237
241	-.0425	-.1685	-.110	-.002125
242	-.0400	-.0782	-.1525	-.001935
243	-.0387	-.0532	-.240	-.00237
244	-.0287	-.1158	-.0951	-.01562
245	-.0275	-.0688	-.0975	-.001875
246	-.0281	-.0500	-.155	-.00213
247	-.0313	-.1375	-.145	-.0025
248	-.0300	-.0640	-.170	-.00275
249	-.0300	-.0422	-.250	-.00300
250	-.0313	-.144	-.185	-.0035
251	-.0312	-.0595	-.240	-.00325

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TABLE III-B (CONCLUDED)
ANTI - SYMMETRICAL CASE

{ CONFIDENTIAL }

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EDR-C905-104

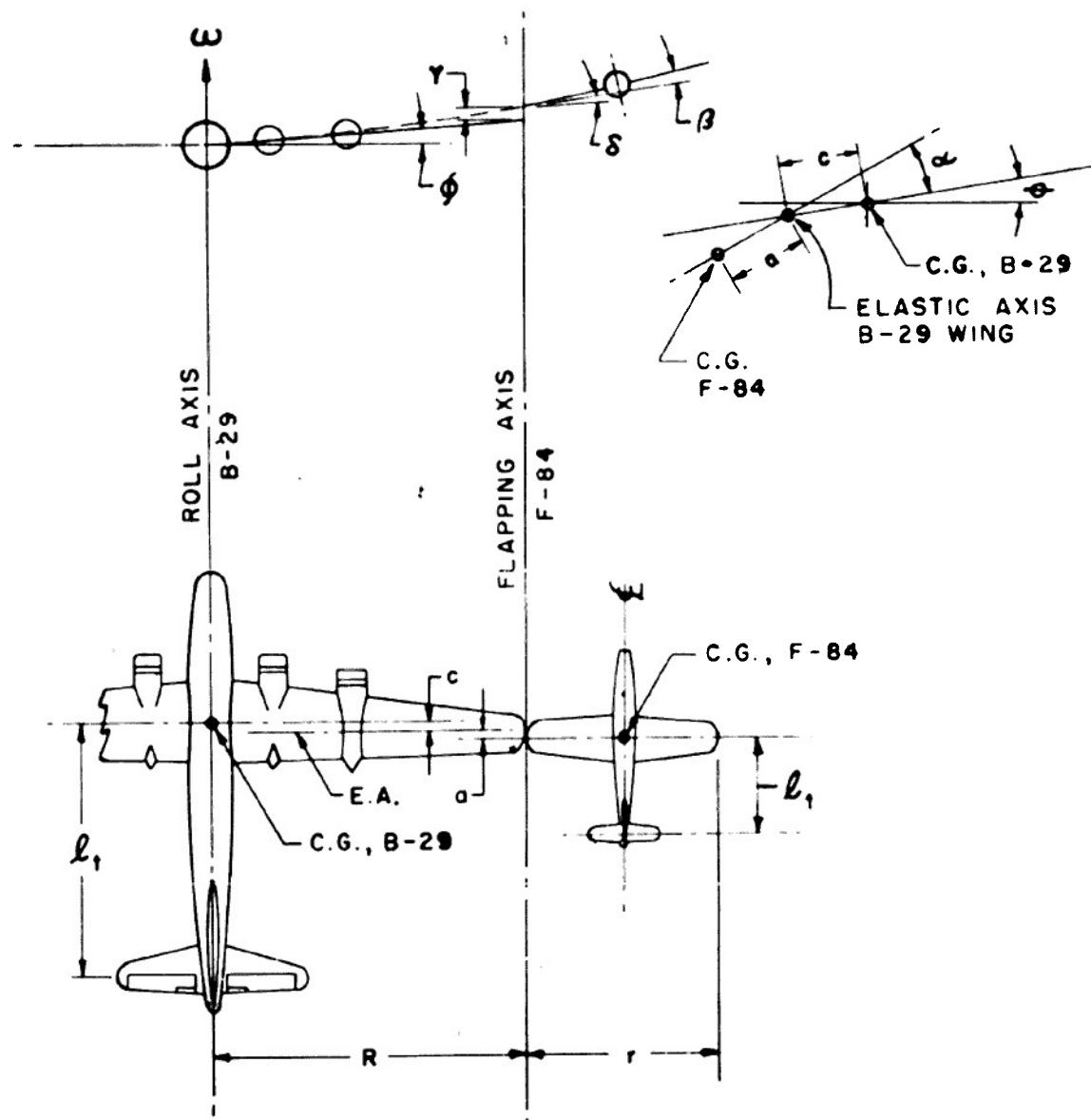
RUN	ψ (RAD. SEC)	β (RAD)	y (FT.)	α (RAD)
252	-.0300	-.0344	-.220	-.00363
253	-.0350	-.075	-.100	-.00175
254	-.0337	-.0814	-.105	-.00312
255	-.0325	-.0562	-.170	-.001875
256	-.0375	-.1565	-.130	-.00244
257	-.0350	-.1375	-.160	-.00213
258	-.0350	-.0532	-.240	-.00250
259	-.0400	-.1935	-.165	-.00375
260	-.0387	-.0751	-.240	-.00287
261	-.0375	-.0475	-.330	-.00337
262	-.0406	-.1875	-.100	-.00212
263	-.0381	-.0906	-.135	-.00212
264	-.0375	-.0625	-.200	-.001875
265	-.0413	-.100	-.120	-.00263
266	-.0400	-.0877	-.160	-.00225
267	-.0387	-.0564	-.240	-.00181
268	-.0375	-.131	-.150	-.00225
269	-.0387	-.0641	-.160	-.00212
270	-.0381	-.0438	-.220	-.00225

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FIGURE I
POSSIBLE MODES OF MOTION CONSIDERED
IN FLEXIBLE WING ANALYSIS
OF WING TIP COUPLING



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08-305-194

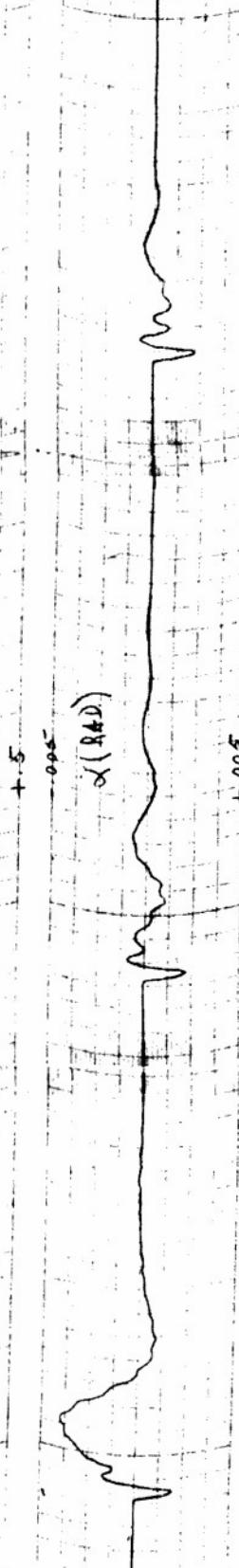
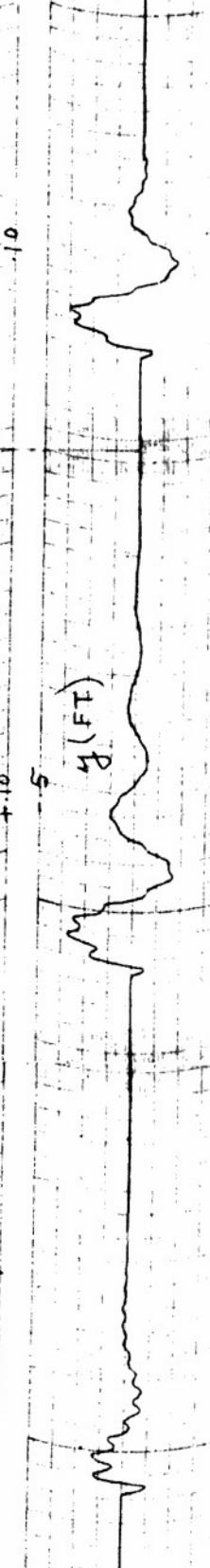
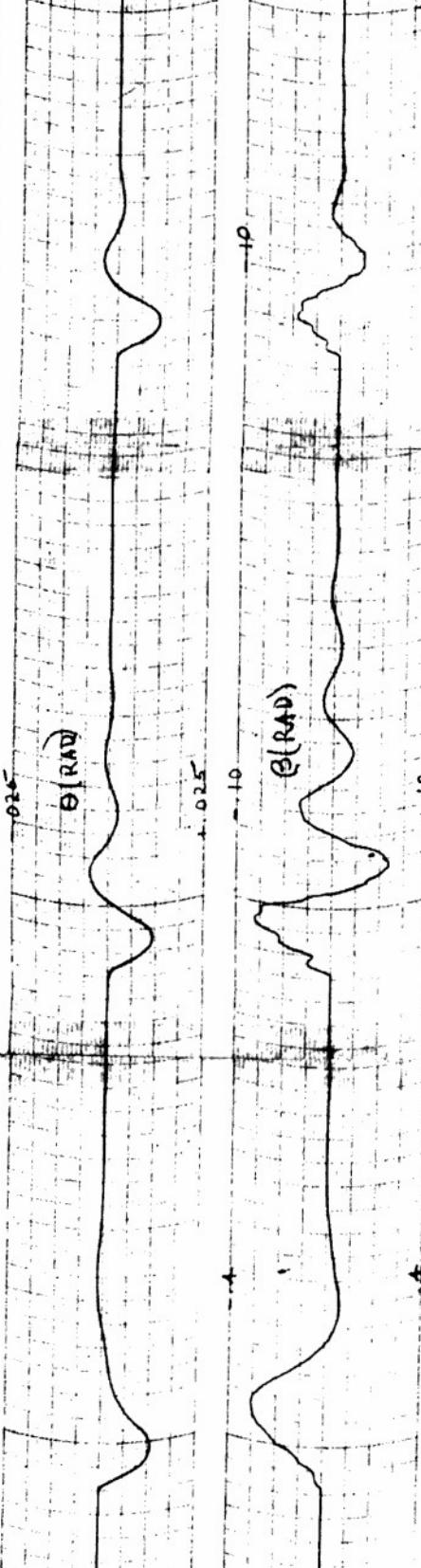
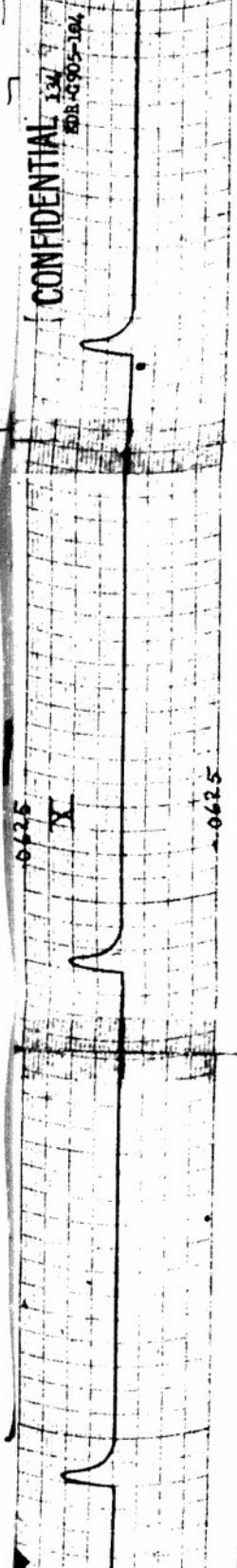


FIGURE II-A
SYMMETRICAL MOTION

RUN # 122

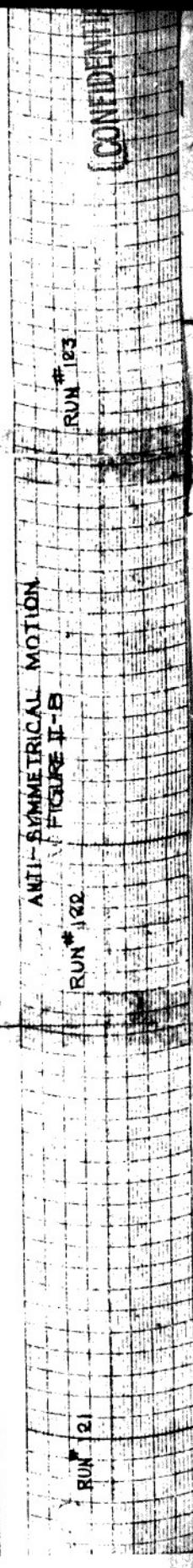
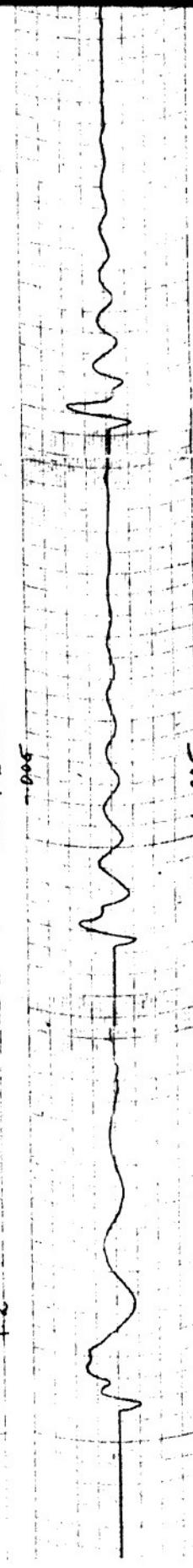
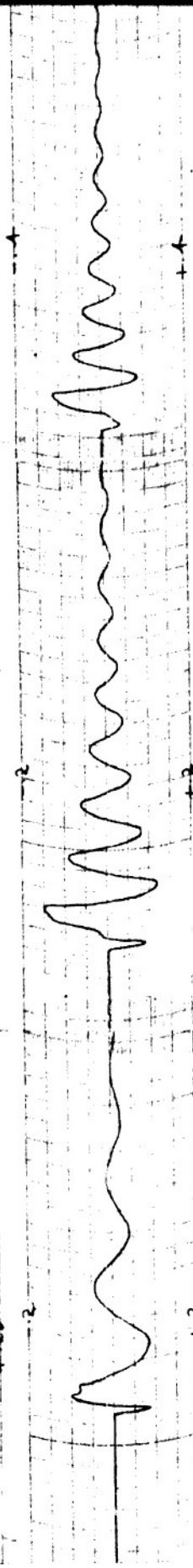
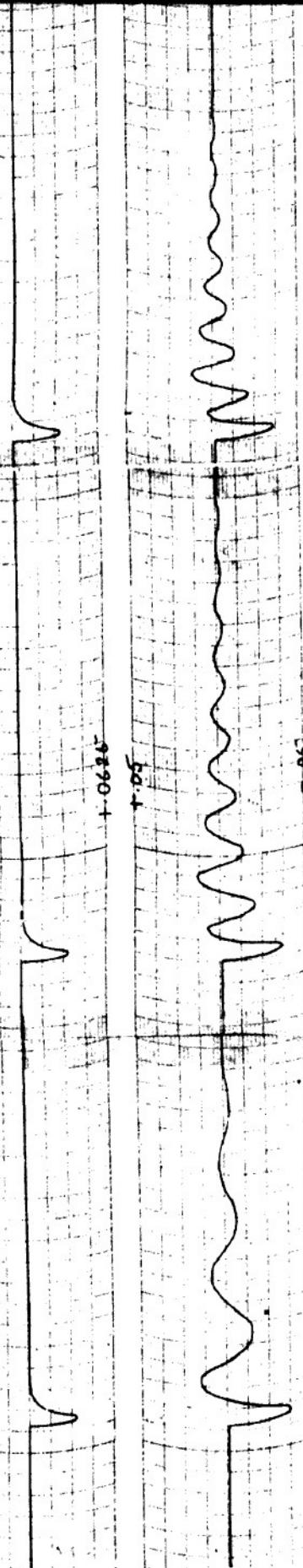
RUN # 121

RUN # 123

CONFIDENTIAL

CONFIDENTIAL

135
35-0925-1A



ANTI-SYMMETRICAL MOTION
FIGURE II-B

RUN # 122

RUN # 123

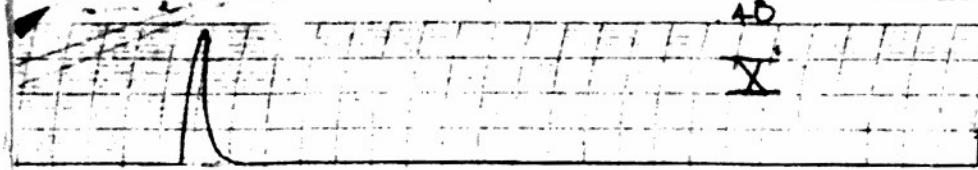
RUN # 123

RUN # 123

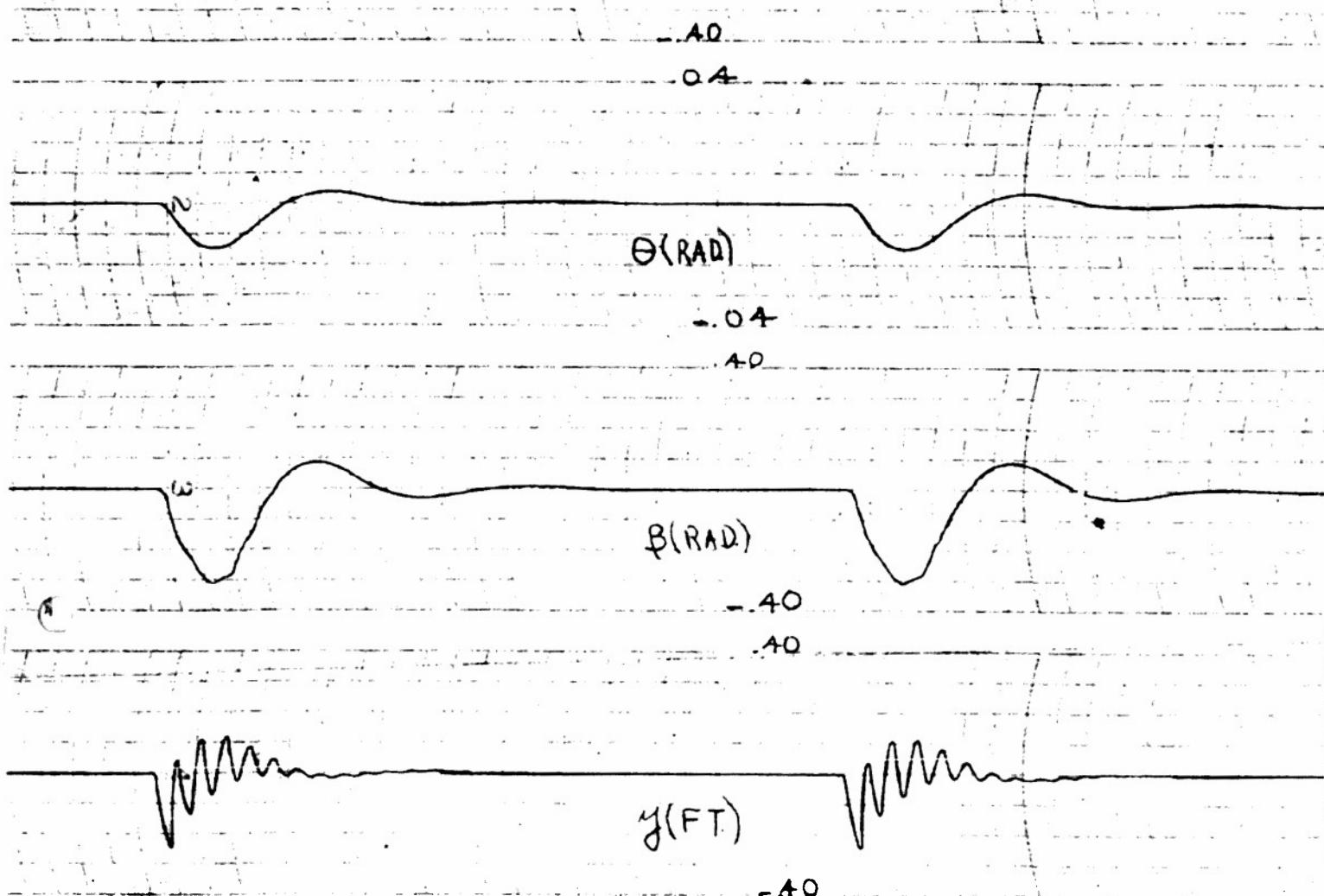
CONFIDENTIAL

CONFIDENTIAL

136
KDR-C 905-104



1 SEC.



SYMMETRICAL MOTION
W TERM ABSENT.
 $K \neq 0$

RUN #86

FIGURE III-A

01

α (RAD)

CONFIDENTIAL

CONFIDENTIAL

137
DR-C905-104

X

40

-0+

α (RAD)

CONFIDENTIAL

-0+

-0+

SYMMETRICAL MOTION
 w TERM PRESENT
 $K=0$

RUN #86

FIGURE III-B

40

-0-

θ (RAD)

-0-

40

β (RAD)

-0-

y (FT)

-0.

40